

SCIENCE APPLICATIONS INCORPORATED

(NASA-CR-144261) DATA ANALYSIS FOR SKYLAB
PROTON SPECTROMETER (Science Applications,
Inc., Huntsville, Ala.) 96 p HC \$5.00

N76-22285

CSCL 14B

G3/19

Unclassified
25257



SAI-77-518-HU

DATA ANALYSIS FOR SKYLAB

PROTON SPECTROMETER

FINAL REPORT

Contract No NAS8-31372

13 April 1976

Prepared by

Charles W Hill

Prepared for

George C Marshall Space Flight Center
Marshall Space Flight Center, Alabama 35812

S C I E N C E A P P L I C A T I O N S, I N C

Suite 800, 2109 W Clinton Avenue
Huntsville, Alabama 35805 (205) 533-5900



FOREWORD

This report is submitted to the George C Marshall Space Flight Center, National Aeronautics and Space Administration, Huntsville, Alabama, in accordance with the requirements of Contract NAS8-31372. The Contracting Officer Representatives are Mr John W Watts (Principal), Dr Tom Parnell (1st Alternate) and Mr R A Gray (2nd Alternate).

John Watts, Space Sciences Laboratory, has made large contributions to this report. His efforts in securing the data, finding and correcting data processing software errors, reprocessing the data tapes, providing calibrations, and day-to-day assisting in data analysis are greatly appreciated.



ABSTRACT

This report examines the data from a proton spectrometer flown aboard Skylab. The instrument is sensitive to protons in the energy range 18 to 400 MeV. A partial failure at the start of the mission was traced to probable failure of the optical coupling between the CsI crystal and the photomultiplier. The loss of all proton counts after several weeks was due to the same cause combined with low temperatures.

The partial failure restricted spectral analysis to two energy bands, 18 to 27 MeV and 27 to 400 MeV. The directional data showed that a Gaussian angular distribution parameter of at least 70° is required for the low energy band and at least 40° for the high energy band. The data, integrated over angle, indicate that the AP3 model extrapolated down to 18-27 MeV is high by factors of 2 to 5 over most of the B-L space mapped. In the 27 to 400 MeV range, the AP3 model is 20 to 100 percent low at low and high values of L, and is high at medium L values in the B-L space mapped.



TABLE OF CONTENTS

	<u>PAGE</u>
Foreword ..	11
Abstract	111
1 Introduction	1-1
2 Flight History	2-1
3 Analysis	3-1
4 Results	4-1
5 References	5-1



LIST OF ILLUSTRATIONS

<u>Figure</u>		<u>Page</u>
1	Spectrometer Schematic	1-2
2	Flux Contour Map of the Skylab Orbit in B-L Space 235 n m - 50°, AP7(3)	3-9
3	R versus σ , 27-400 MeV $0 < B' < 005$	4-3
4	R versus σ , 27-400 MeV $005 < B' < 01$	4-5
5	R versus σ , 27-400 MeV $01 < B' < 02$	4-7
6	R versus σ , 18-27 MeV $0 < B' < 005$	4-10
7	R versus σ , 18-27 MeV $005 < B' < 01$	4-12
8	R versus σ , 18-27 MeV $01 < B' < 02$	4-14
9	R (summed over Pitch Angle) versus σ $0 < B' < 005$	4-17
10	R (summed over pitch angle) versus σ $005 < B' < 01$	4-18
11	R (summed over pitch angle) versus σ $01 < B' < 02$	4-19



LIST OF TABLES

<u>Table</u>		<u>Page</u>
A1	Ratio of Measured to Model Counts as a Function of B' , L' , and α	A1-1
A2	Ratio of Measured to Model Counts as a Function of B' and L'	A2-1
A3	Ratio of Measured to Model Counts in the East and West Directions as a Function of B' and L'	A3-1



1 0 INTRODUCTION

A proton spectrometer, sponsored by the Space Sciences Laboratory, George C Marshall Space Flight Center, NASA, was placed aboard the Skylab vehicle. The Principal Investigator was Dr Godehart Guenther, University of Alabama in Huntsville. This report presents an analysis of the data obtained during the first dozen days of the mission.

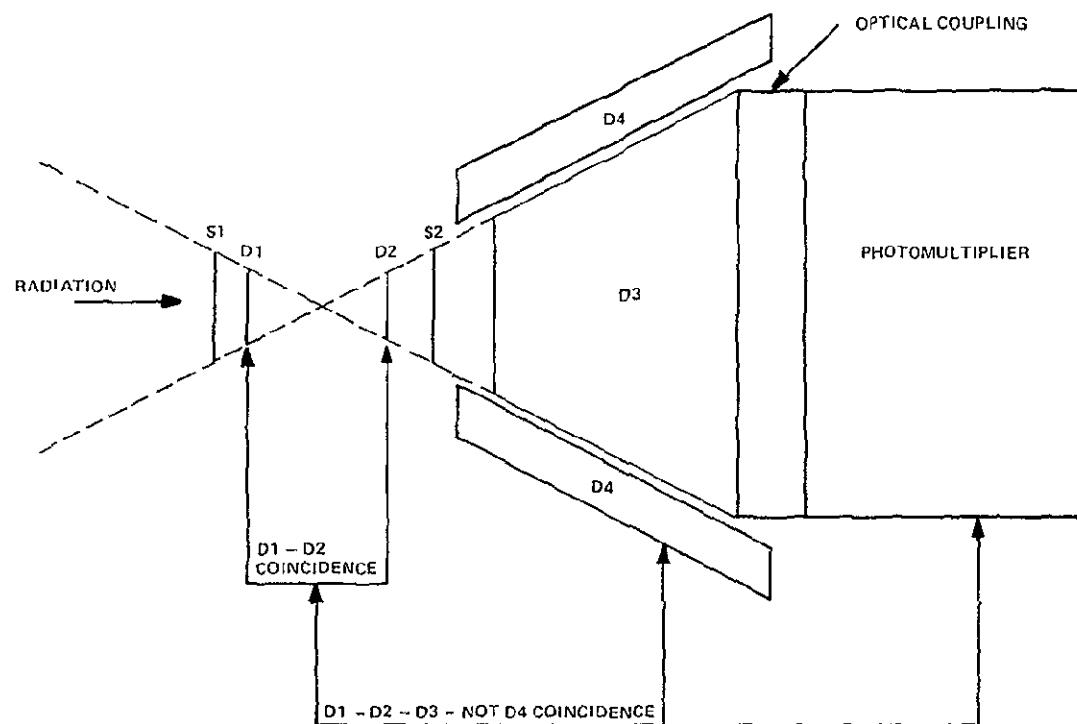
Proton radiation fluxes were sampled four or five times per day as the Skylab cluster penetrated the South Atlantic anomaly. The orbit altitude was 450 km at 50 degree inclination.

The proton spectrometer has been described in other articles^(1,2). A brief description is given here for familiarization purposes.

The spectrometer is designed to discriminate against a large electron background. A collimator and detector telescope arrangement limit the acceptance cone to a 22.5 degree half angle as shown in Figure 1. Protons enter the instrument through an outer shield, S1, which reduces the low energy electron flux. D1 and D2 are solid state detectors with a 10 nanosecond coincidence requirement. These detectors define the acceptance cone and help ensure that single particles are being examined. In addition, an energy threshold requirement of 400 KeV is imposed on D2 to discriminate against electrons.

A proton which penetrates D1 and stops in D2 has 18 MeV. This is the low energy boundary on the first proton channel. A proton which penetrates a second shield, S2, with less than 250 KeV possesses 27 MeV. This defines the upper energy boundary of the first proton channel.





SAI 0561

Figure 1 Spectrometer Schematic

Protons with energy greater than 27 MeV will deposit more than the 250 KeV threshold energy in the thallium-activated, cesium iodide detector, D3. Another coincidence between D3 and the two solid state detectors is required. Protons between 27 and approximately 150 MeV will be stopped in D3. These protons deposit more than one MeV in D2, thus setting a "high" flag in the logic circuits. Protons between 150 and 400 MeV deposit 0.4 to 1.0 MeV in D2 and set a "low" flag in the logic circuits.

Light generated in the CsI D3 detector is transmitted to a photomultiplier tube through a light coupling material. The amplified signal is sent to an analog-to-digital converter (ADC) which generates a wave train with the number of pulses proportional to the energy deposited. Another circuit counts the pulses, examines the "high" "low" flag, and increments the counter in one of seven energy channels (channels 2-8).

Spurious counts and energies entering from the side are discriminated against by requiring an anticoincidence from a plastic guard detector, D4.

Details of other special features such as an accidental coincidence counter are available in previous reports^(1,2).



20 FLIGHT HISTORY

The proton spectrometer suffered a partial failure either during the launch or during the low temperature period after Skylab achieved orbit and before the instrument was turned on. The meteoroid/insulation shield around the Workshop ripped off during the powered phase of the launch. One of the solar panel wings was also lost. The other solar panel wing was jammed until the first Skylab crew managed to free it several weeks later.

Fortunately, some power was available from the Apollo Telescope Mount solar panels. This power was rigorously conserved by shutting down all nonessential equipment including the proton spectrometer. Because the spectrometer is mounted externally on the anti-solar side near the top of the Multiple Docking Adaptor (MDA) and because it is thermally isolated from the MDA structure, the temperature inside the instrument fell to about -40°F .

Eventually, two decisions were made which brought the instrument temperature up into its operating range. One decision caused the spacecraft to be rolled and tilted in an effort to shade the Workshop by the ATM solar panels. The Workshop temperature was climbing to about 120°F at that time. This movement brought the instrument into the sunlight. The other decision which helped raise the temperature was to activate the instrument because it used only 5 watts with the heaters on. The temperature rose to $35 - 40^{\circ}\text{F}$. Several weeks later after repairs were made and the spacecraft was placed in the solar-inertial mode again, the temperature fell below zero, suggesting that the heaters were undersized or that the insulation was damaged in a manner not apparent to the crew during their fly-around survey.



REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

It was difficult to determine the condition of the spectrometer immediately after it was turned on. Radiation was encountered during passage through the South Atlantic anomaly and the horns of the outer belt sporadically during the day. These data were taped and telemetered to ground stations at intervals. The data were placed into a large data base where it could be accessed through the MOPS system. After 24 hours the data were moved to permanent storage where access was difficult. The spectrometer data were available in several displays and in several formats. It was quickly determined that the D4 count rate from the guard scintillator and the D3 total dose from the cesium iodide crystal were behaving as expected. Software errors prevented access to detailed data for several days. After corrections to the MOPS software were made, a small quantity of data became available which indicated the high energy proton channel contained a suspiciously large number of counts relative to the other channels.

Several weeks after mission start, the spacecraft was placed in the solar inertial mode. The temperature in the spectrometer fell to -20°F, and the proton counts ceased. Other spectrometer functions such as D4 count and D3 total dose remained operational.

An attempt was made to analyze the early proton data. Unfortunately, the programs which had been designed to strip out the spectrometer data from the telemetry contained errors which rendered the formatted data meaningless. The software group responsible for those programs had been reassigned to more urgent projects. Eventually the programs were corrected. By this time a torrent of data was coming in from Skylab, threatening to saturate computer facilities and personnel.

A command decision was made to defer all reprocessing requests until after mission completion. The data were reprocessed and made available for analysis early in 1975.

Initial examination of the data showed that it had not operated properly. An informal fault analysis committee was convened by Dr. Tom Parnell, Division Chief, Cosmic Ray Physics, Space Sciences Laboratory (SSL), MSFC. Other members included Dr. Godehart Guenther, Principal Investigator, John Watts, SSL, George Detko, SSL, and Charles Hill, Science Applications, Inc.

The fault was isolated to the optical coupling between the D3 cesium iodide crystal and the photomultiplier tube. This optical coupling is a transparent, rubber-like gel which seals the two interfaces with the aid of a slight mechanical compression. The compression was adjusted to give an operating range of 10 to 90°F. It is probable that part of the seal was affected by the vibration of launch and/or by the cold soak suffered by the spectrometer.

Loss of part of the seal lowers the effective gain of the instrument by reducing the amount of light going to the photomultiplier tube. The flaw is intermittent in nature, as evidenced by the behavior of the self-calibration mode.

The self-calibration feature is based on an Americium source embedded in the D3 cesium iodide crystal. Normally, the signal from this source is below the threshold set on the counting train (ADC). During self-calibration, the gain is increased to such an extent that counts enter channels 2 and 3. Counts are accumulated until either channel 2 or 3 overflows at 1024 counts. If the other channel is below a predetermined value, the gain is stepped up or down towards the balance point. The process is then repeated. A total of 16 gain steps are available covering approximately 30 percent total gain change.



During operation the gain changes would often be stable for a period of time, then change rapidly over a five minute interval. The non-overflowing channel would fall from over 900 counts to very low values, usually about 100 but sometimes down to 5. The allowable gain change could not compensate for the intermittent loss of gain probably caused by defects in the optical interface. Restoral of gain often took place within 5 minutes. After several weeks, the count rate fell to zero.

An effort has been made to salvage usable data from the proton spectrometer. Recalibration was not possible due to the fluctuating nature of the defect. Eventually a two-band analysis was chosen because more detailed spectral analysis was impossible.

The low band energy range is 18 to 27 MeV. Protons in this range may penetrate the first absorber and the D1 and D2 solid state detectors which define the acceptance angle, but are stopped in the second absorber before reaching the D3 crystal. The high energy band range is approximately 27 to 400 MeV. These protons stop in or completely penetrate the D3 crystal.

The low energy band is not significantly affected by the defect because the D3 crystal is not involved. The low energy end of the high band is slightly affected. The spectrometer is designed so that 27 MeV protons entering the acceptance cone will deposit about 250 KeV in D3. A threshold discriminator is set to reject signals below 250 KeV. The gain loss during fluctuations is estimated to be about 50 percent. Thus the lower limit may be approximately 27.25 rather than 27.0 MeV. This shift is comparable to fuzziness due to non-uniformity of absorbers and variation of absorber thickness.



due to angle of incidence. The high energy end may be shifted somewhat more, perhaps 10 MeV. This shift is comparable to other uncertainties such as the angle of incidence effect. Also, the environment contains relatively few protons near 400 MeV.

For the above reasons, the nominal energy limits of the upper band are unchanged. Unfortunately, it is impossible to unscramble the 7 energy channels in the upper band so they are simply added together in this study.



3 0 ANALYSIS

The proton spectrometer is a directional instrument. The proton flux is anisotropic with very small intensity parallel to the magnetic field lines and maximum intensity perpendicular to the field lines. Therefore, the analysis requires the altitude, latitude, and longitude of the Skylab cluster at the time of a measurement, the pointing direction of the spectrometer, and the direction of the field lines.

The experimental data is compared to the Vette AP3 proton environment model⁽³⁾ for omnidirectional flux above 30 MeV. A computer program finds the AP3 model omnidirectional flux, applies a range of assumed pitch angle distributions to the flux model, folds in instrument response, and computes the values which would be seen by an idealized proton spectrometer immersed in the AP3 model environment.

The direction cosines of the spectrometer pointing vector are (0, -1, 0) in the MDA coordinate system. This direction is related to a system rotating with the earth through the application of 6 rotation transformations.

$$\begin{pmatrix} PS1 \\ PS2 \\ PS3 \end{pmatrix} = F E D C B A \begin{pmatrix} 0 \\ -1 \\ 0 \end{pmatrix}$$

Here (PS1, PS2, PS3) are the desired direction cosines of the proton spectrometer axis in the rotating earth coordinate system at the time of the measurement.

Transformation A relates the MDA system to the OWS system, accounting for bending at the flexible Airlock-OWS coupling. The transformation is derived from Skybet tape Euler angles (E1, E2, E3). The result of the first transformation is as follows:



$$PSOWS1 = \cos E1 \cos E2 \sin E3 - \sin E1 \sin E2$$

$$PSOWS2 = -\cos E1 \cos E3$$

$$PSOWS3 = -\cos E1 \sin E2 \sin E3 - \sin E1 \cos E2$$

Matrix B transforms from the OWS system to the ECI (Earth Centered Inertial, of date 1950 0) system. The Z-axis of the ECI system points along the north pole of the spin vector. The X-axis is toward the vernal equinox. In terms of the SKYBET-furnished Euler angles, (U1, U2, U3), the B matrix is as follows. Note that CU1 = cos U1 and SU1 = sin U1, etc.

$$B = \begin{pmatrix} CU3 & CU2 & -CU1 & SU3 & CU2+SU1 & SU2 & +SU1 & SU3 & CU2+CU1 & SU2 \\ +SU3 & CU1 & CU3 & & & & -SU1 & CU3 & & \\ -CU3 & SU2 & CU1 & SU3 & SU2+SU1 & CU2 & -SU1 & SU3 & SU2+CU1 & CU2 \end{pmatrix}$$

Matrix C transforms a column vector in ECI (epoch 1950) to ECI (epoch 1973) coordinates. It is a precession correction. Matrix C is furnished by the Dudley Observatory, Albany, New York. It was checked against Transformation 33, pp 418-419, of Methods of Orbit Determination, Escobal, John Wiley & Sons, Inc., New York, 1965, and found identical to within two units in the seventh place after the decimal.

$$C = \begin{pmatrix} 99998 & 42912 & -00514 & 04016 & -00223 & 46372 \\ 00514 & 04016 & 99998 & 67880 & -00000 & 57437 \\ 00223 & 46372 & -00000 & 57433 & 99999 & 75032 \end{pmatrix}$$

Matrix D corrects for nutation (wobble) from ECI (epoch 1973) to ECT (Earth Centered True, epoch 1973). This small correction is based on observational data and may be computed only after the fact. Matrix D is furnished by the Dudley Observatory.

$$D = \begin{pmatrix} 99999 & 99968 & -00007 & 37907 & -00003 & 19975 \\ 00007 & 37903 & 99999 & 99972 & -00001 & 09138 \\ 00003 & ,19983 & 00001 & 09114 & 99999 & 99994 \end{pmatrix}$$



Matrix E rotates the ECT coordinate system around the Z-axis so that the X-axis is moved from the vernal equinox to the Greenwich meridian

$$E = \begin{pmatrix} \cos \theta & \sin \theta & 0 \\ -\sin \theta & \cos \theta & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$\theta = 99\ 6909833 + 36000\ 7689 \text{ TU} + 00038708 \text{ TU}^2$$

TU = elapsed time in Julian centuries, or

$$\text{TU} = (2441682.5 - 2415020) / 36525$$

A half day has been subtracted to change from Greenwich noon, Jan 0, 1950, to 0 hr, 0 min, Jan 0, 1973

Matrix F corrects from ECT (1973 0) to the time of measurement

$$F = \begin{pmatrix} \cos wt & \sin wt & 0 \\ -\sin wt & \cos wt & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

t = time since 0 hr, 0 min, Jan 0, 1973

w = 26251.61453 radians/hr

The six rotations shown above convert the PS axis from the local MDA system to the rotating earth system

The counts in proton channels P1-P8 are screened for validity. Total counts fewer than 5 distributed among the 8 channels during a 1/2 second period are discarded. Counts greater than 50 in a single channel indicate a probable error and that period is discarded. The counts are normalized to counts per second and dead time corrections are applied. These calculations are made at each measurement point, i.e., every 1/2 seconds along the trajectory where sensible flux is encountered. The measured values and calculated values are summed over time, then ratioed to provide spectral correction factors.



At the same time, the data are tabulated according to location (B , L), pitch angle (α), energy, assumed pitch angle distribution (σ), and orientation in the earth-fixed coordinate system (θ_{LV}, ψ_{LV}) With the aid of this data, detailed corrections to the AP3 model environment are derived "Best fit" energy-dependent pitch angle distributions are also obtained Finally, some information is derived concerning the east-west asymmetry, though this effect is blurred at higher energies due to acceptance in the backward cone of the PS above 100 - 150 MeV

The Vette AP3 flux parameters, a and b , are found by table look-up using values of B and L from the SKYBET tape

$$AP3\ FLUX\ (>E) = aE^{-b}$$

This form is differentiated, and the resultant is integrated over energy ranges corresponding to those of the eight proton channels The angle α between the local magnetic field line, B , and the axis of the PS primary cone is found using the scalar product The angle α is used in a table look-up to determine that fraction of the AP3 omnidirectional flux which would be observed by an ideal PS The measured angular response of the instrument is triangular, peaked on the axis and going to zero at $\pm 22.5^\circ$ The assumed pitch angle distribution is Gaussian

$$\frac{-(90-\alpha)^2}{e^{2\sigma^2}} \\ \frac{1}{\sigma\sqrt{2\pi}}$$

The idealized instrument reading is obtained by numerical integration and condensed into tables for this program Note that σ determines the angular distribution of the flux A set of 10 values are chosen for σ so that parallel calculations may be made



The flux values computed above will be denoted by Φ^* . Each quantity will be further identified by two sets of subscripts

The first set of subscripts is described as follows

$$\Phi_{ijkl}^*, \Phi_{ijklm}$$

where

$$i = B' \text{ (note prime)}$$

$$j = L' \text{ (note prime)}$$

$$k = \alpha$$

$$l = E$$

$$m = \sigma$$

Figure 2 shows that rectangular boxes in $B - L$ coordinates would be wasteful of computer storage, or would have large variations in flux level within a box. Therefore, a transformation is applied to obtain $B'-L'$ coordinates which are better suited here.

$$\begin{pmatrix} B' \\ L' \end{pmatrix} = \begin{pmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{pmatrix} \begin{pmatrix} B \\ L \end{pmatrix} + \begin{pmatrix} -1348 & 0423 \\ -11589 & 3780 \end{pmatrix}$$

$$\theta = -3^\circ 5' 10''$$

The B' box limits are 0- 005, 005- 01, 01- 02, and > 02. The L' box limits go from 0 to 7 in steps of 1, then > 7.

The box limits in the α dimension are 0 - 30, then 10 degree steps to 90 degrees. Angles greater than 90° are reflected back to the first quadrant.

The box limits in the energy dimension are 18-27, 27-400, and 18-400 MeV.



The calculated fluxes, Φ , have an extra dimension, pitch angle distribution σ , and 10 parallel calculations are made for this quantity. The assumed pitch angles parameters are 5, 10, 15, 20, 25, 30, 40, 50, 60 and 70 degrees.

A second set of subscripts and tables is necessary for the east-west asymmetry study. These subscripts are

$$\Phi^*_{1jln1n2}, \quad \Phi^*_{1jlmn1n2}$$

where

$$\begin{array}{ll} i = B' & m = \sigma \\ j = L' & n_1 = \theta_{LV} \\ l = E & n_2 = \psi_{LV} \end{array}$$

The σ subscript, k , is replaced by two subscripts, n_1 and n_2 , identifying equal solid angle boxes in the Local Vertical system. Here n_1 labels the polar angle with boundaries at 0, 60, 90, 120 and 180°, while n_2 labels the azimuthal angle with limits at 330, 30, 90, 150, 210, and 270°. The solid angle is subdivided into $4 \times 6 = 24$ equal size boxes. Here, the measured fluxes, Φ^* , are tabulated in a 5-dimensional table.

Values of Φ^* , Φ^{*2} , Φ and Φ^2 are determined for each measurement (1/2 seconds) and are accumulated in separate tables according to the two sets of subscripts described above. Auxiliary tables are compiled to show the number of entries in each box of each table.

The tables described above are too lengthy to keep in fast storage. Therefore, Φ^* , the 10 Φ 's, and the two sets of subscripts are placed in a buffer. When the buffer is full, it is dumped into mass storage. After the input tape is processed, the values are brought back into fast core and processed. The subscripts, maximum value, and quantity represented are listed below.



1 8 E	m 10c
J 8 L'	n2 6 ψ_{LV}
1 4 B'	n1 4 θ_{LV}

The measured and calculated data are sorted into tables as described above. Later, the 8 energy channels are collapsed into the 3 energy bands described previously due to the partial spectrometer failure. The cumulative tables are stored on tape in the following order.

Number of Entries Tables

- 1 Number of entries per bin for the pitch-angle tables
(8 E's, 8 L's, 4 B's, 7 α 's = 1792 words)
- 2 Number of entries per bin for the east-west tables
(8 E's, 8 L's, 4 B's, 6 azimuthal angles,
4 polar angles = 6144 words)

Pitch-Angle Tables

- 3 Measured pitch-angle, Φ^* , 1792×2 words (Φ^*, Φ^{*2})
- 4-13 Calculated pitch-angle for 10 assumed distributions,
 Φ_m , $10 \times 1792 \times 2$ words (Φ_m, Φ_m^2)

East-West Tables

- 14 Measured east-west table, Φ^* , 6144×2 words
- 15-24 Calculated east-west tables for 10 assumed distributions, Φ_m , $10 \times 6144 \times 2$ words

The total table storage is 182528 words

Values are accumulated over each pass through the South Atlantic anomaly, then added to previous accumulations. Within each box, the summed values are

$$\begin{array}{ll} T = \Sigma \Phi^* & S = \Sigma \Phi \\ T_2 = \Sigma \Phi^{*2} & S_2 = \Sigma \Phi^2 \end{array}$$



The mean value of the measured flux within a box is T/n , where n is the number of entries in that box. A standard deviation is defined herein (incorrectly) to be identical with the root mean square deviation. The reason for this simplification is to reduce the alternate computations required when $n = 1$.

$$\begin{aligned}(S_D)^2 &= \frac{1}{n} \sum (\Phi^* - \bar{\Phi}^*)^2 \\ &= \frac{1}{n} \sum (\Phi^{*2} - \bar{\Phi}^{*2}) \\ &= \frac{1}{n} T^2 - \frac{1}{n} \frac{1}{n} (T)^2\end{aligned}$$

Thus

$$(S_D) = \sqrt{\frac{nT^2 - T^2}{n}} \text{ and the fractional } (S_D) \text{ is } (F_S D) = \sqrt{\frac{nT^2 - T^2}{nT^2}} / T$$

for the measured flux within a box. Similar expressions may be derived for the model fluxes.

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR



Flux units are

$$\frac{p(E > 50 \text{ MeV})}{\text{cm}^3 \cdot \text{sec}}$$

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

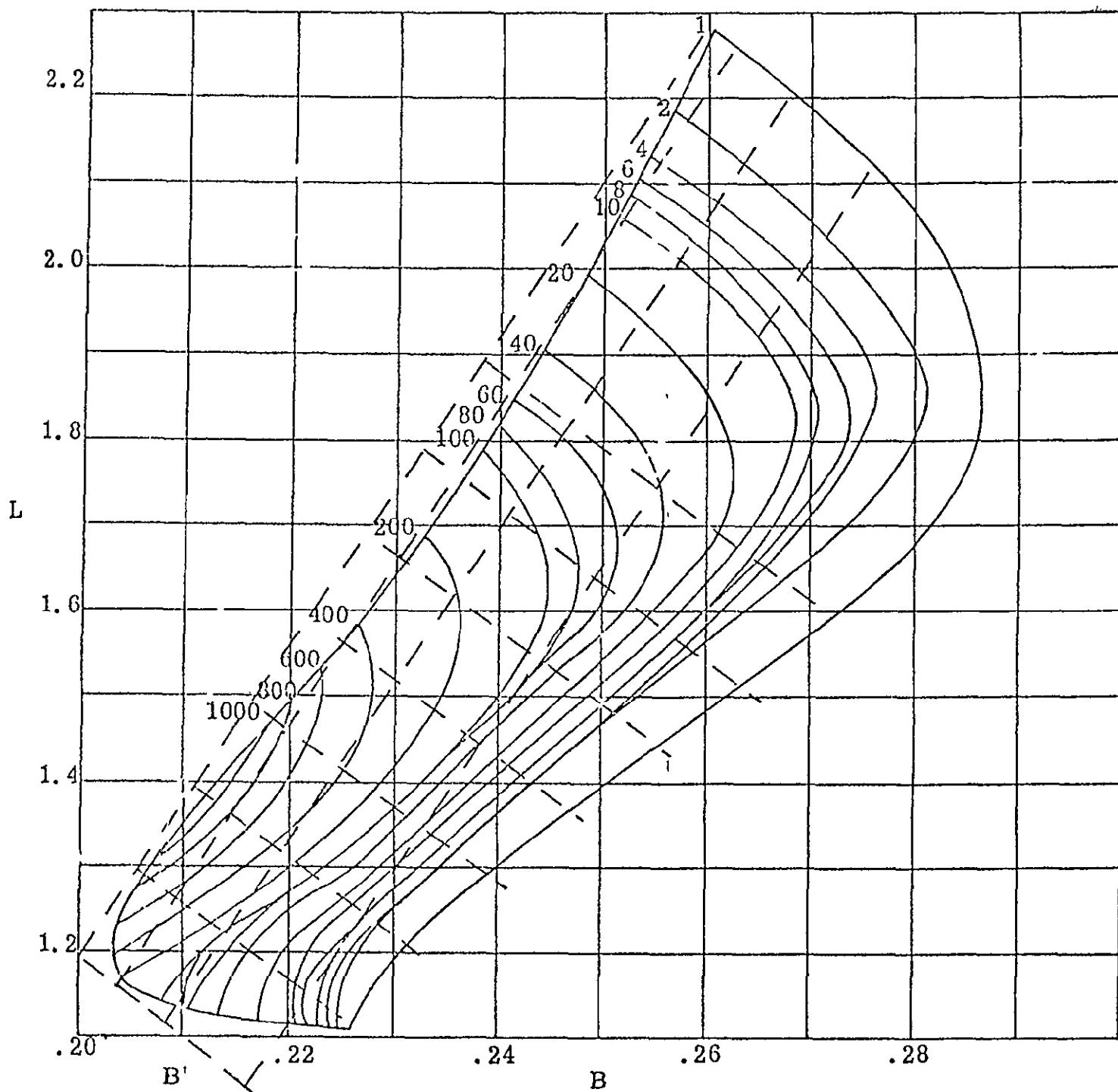


Figure 2 Flux Contour Map of the Skylab Orbit in B - L Space
235 n. m. - 50°, AP7⁽³⁾

4 RESULTS

The results of the analysis are shown in Tables A1, A2, and A3. Table A1 gives the ratio, R, of the measured flux to the model flux within each B' , L' , α (I, J, K) box. Table A2 shows similar ratios after weighted summing over the pitch angle, α . Table A3 shows the ratio of measured to model flux coming from the east hemisphere and the west hemisphere within each B' , L' box.

Within each table, data are presented for 3 energy groups, 18-27, 27-400, and 18-400 MeV. The measured fluxes are compared to the AP3 model fluxes⁽³⁾ which are intended for use above 30 MeV. Therefore, attention should be focused upon the center band (27-400 MeV). An attempt was made to use the newer AP7 proton environment model⁽³⁾ (valid above 50 MeV), but this model does not extrapolate well down to 27 MeV. It may be noted that the AP3 and AP7 spectra, integrated over the entire orbit, are nearly identical above 50 MeV for the Skylab trajectory.

The data are taken from 3280 samples of 1/2 seconds each, or about 66 minutes of active measurement. This data represents less than 2 percent of the data sought. Of the 224 B' , L' , α boxes, 81 contain samples, averaging 40 samples per box.

Table A1 contains 10 sets of ratios. The first, labeled "M=1", assumes a 5 degree parameter in the AP3 angular distribution model. This parameter increments by 5 degrees to 30, then 10 degrees to 70. The first set uses a flux model sharply peaked near the perpendicular to the magnetic field line. This model predicts counts only when α is near 90 degrees, $K=5, 6$, or 7 . The ratio, R, of measured to model



counts is often large for the K=5 boxes, which indicates the model counts are too small. The zero values of R indicate that the ratios are so large that certain program constraints are exceeded. The values labeled "FSDI" are fractional standard deviations (fsd) for the model counts. The values labeled "PFSDI" are fsd's for the measured counts within a box.

Consider the 27-400 MeV results for M=1 ($\sigma=5^\circ$). The model flux angular distribution is obviously too narrow. The ratio R is nearly reasonable only for K=7 and 6 where the spectrometer sees the maximum flux. The R values range from 0.286 to 1.267 for K=7. For K=5 (20-30 $^\circ$ from the l) the model counts become too small and the ratio too large (11 to 953).

At M=5 ($\sigma=25^\circ$), the number of zero ratios is 11 compared to 33 at M=1. Most of the other ratios lie between 0.5 and 3. A few are still large, particularly for K=2 ($30^\circ < \alpha < 40^\circ$), where R lies between 2.2 and 23.2. It is evident that the real flux is again more smeared than the model flux.

At M=6 ($\sigma=30^\circ$), the number of zero ratios is 6 and 7 values of R are greater than 6.0. Most of the large or zero (very large) values of R are for observations within 30 degrees of the field line. The model is still predicting fluxes much smaller than those observed.

At M=7 ($\sigma=40^\circ$), the number of zero ratios in the 27 to 400 MeV range is one and only 3 values of R are larger than 3.0. The zero ratio box contains 2 samples. The ratios larger than 3.0 contain 5, 6, and 15 samples.

This group of data shows some degree of consistency between the experimental and model data. The assumed model data is smeared enough ($\sigma=40^\circ$) to simulate experimental measurements.

Smaller values of σ cause large values of R at small pitch angle as shown in Figures 3, 4, and 5. Figure 3 is a



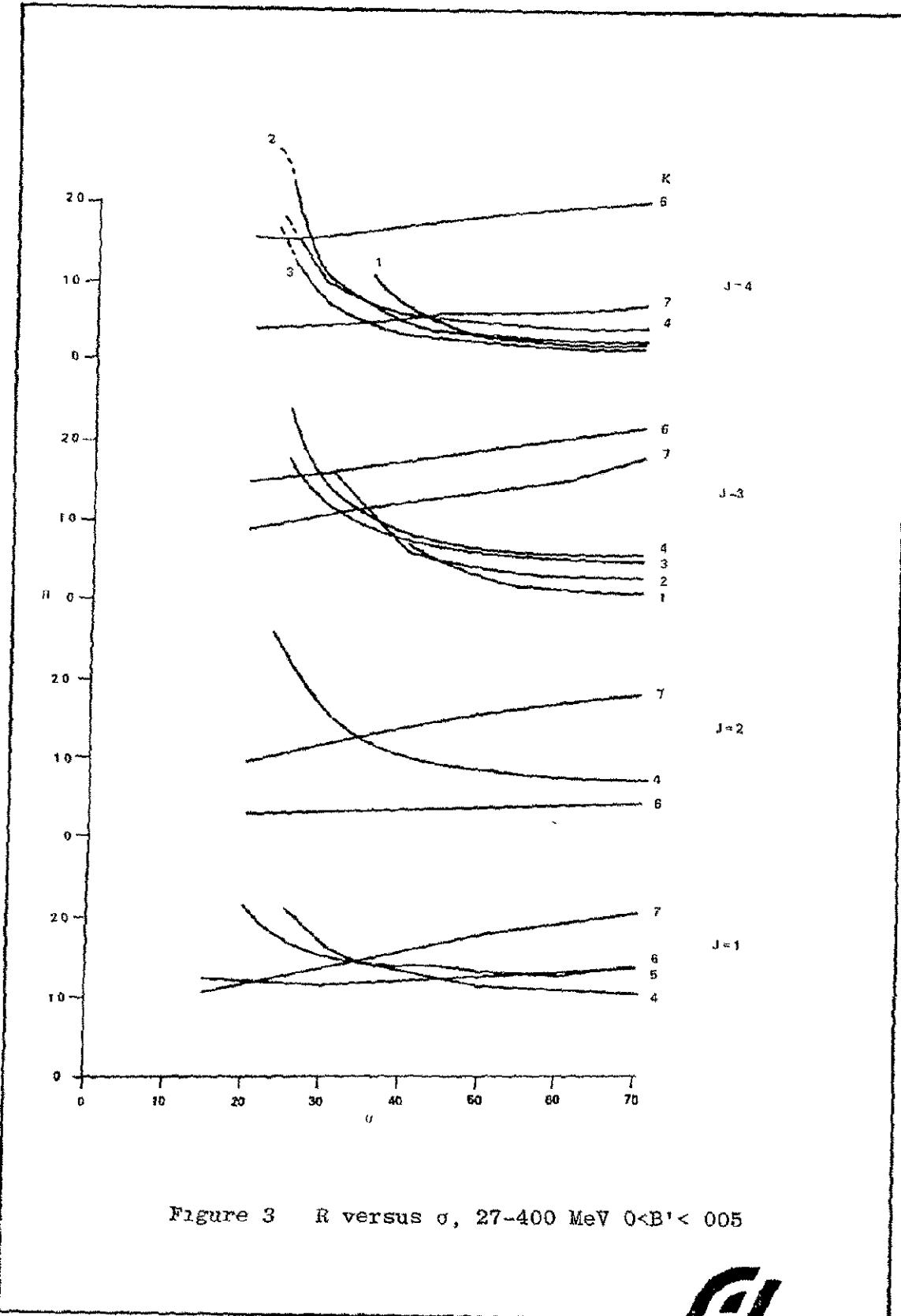


Figure 3 R versus σ , 27-400 MeV $0 < B' < 0.05$

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

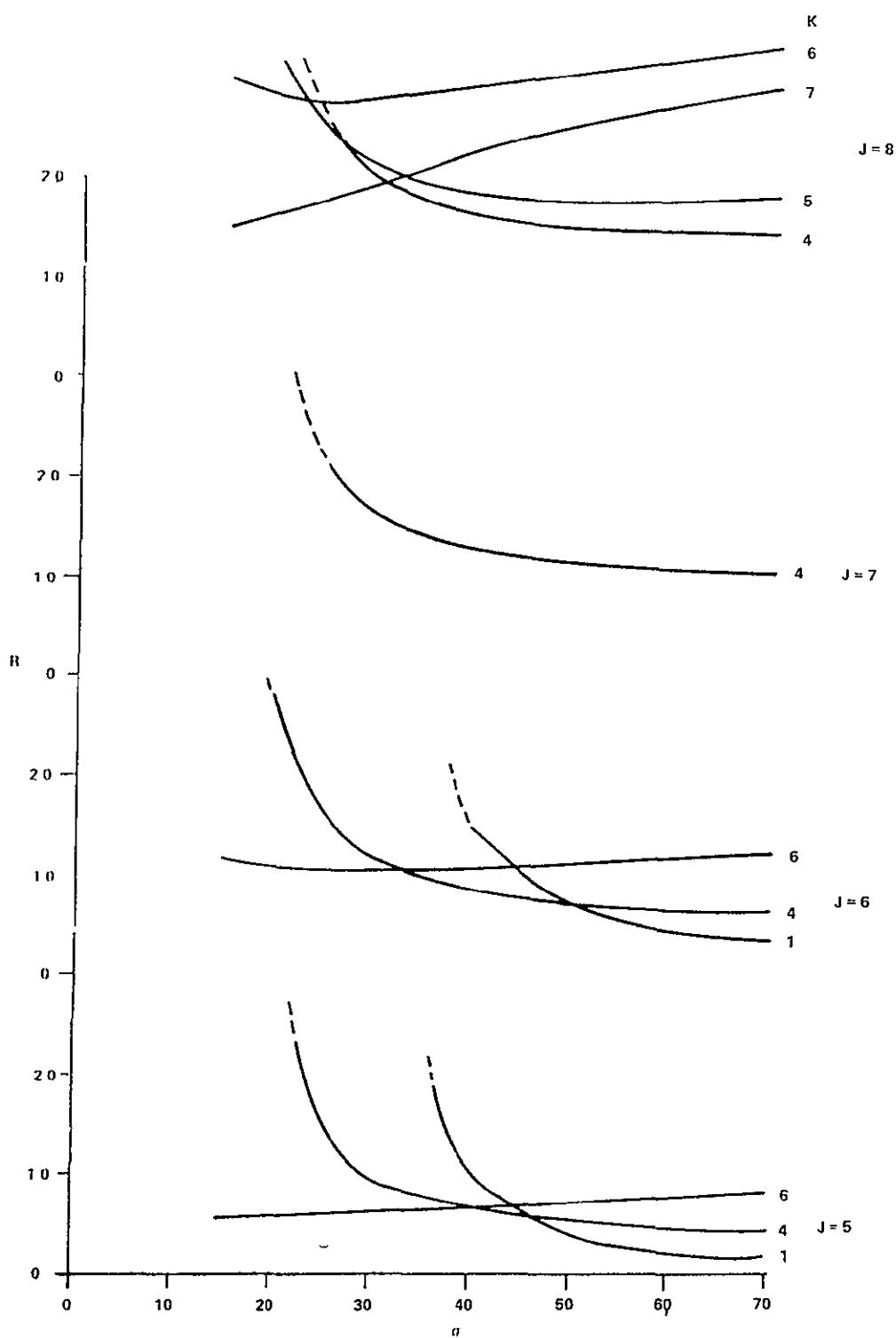


Figure 3. Continued

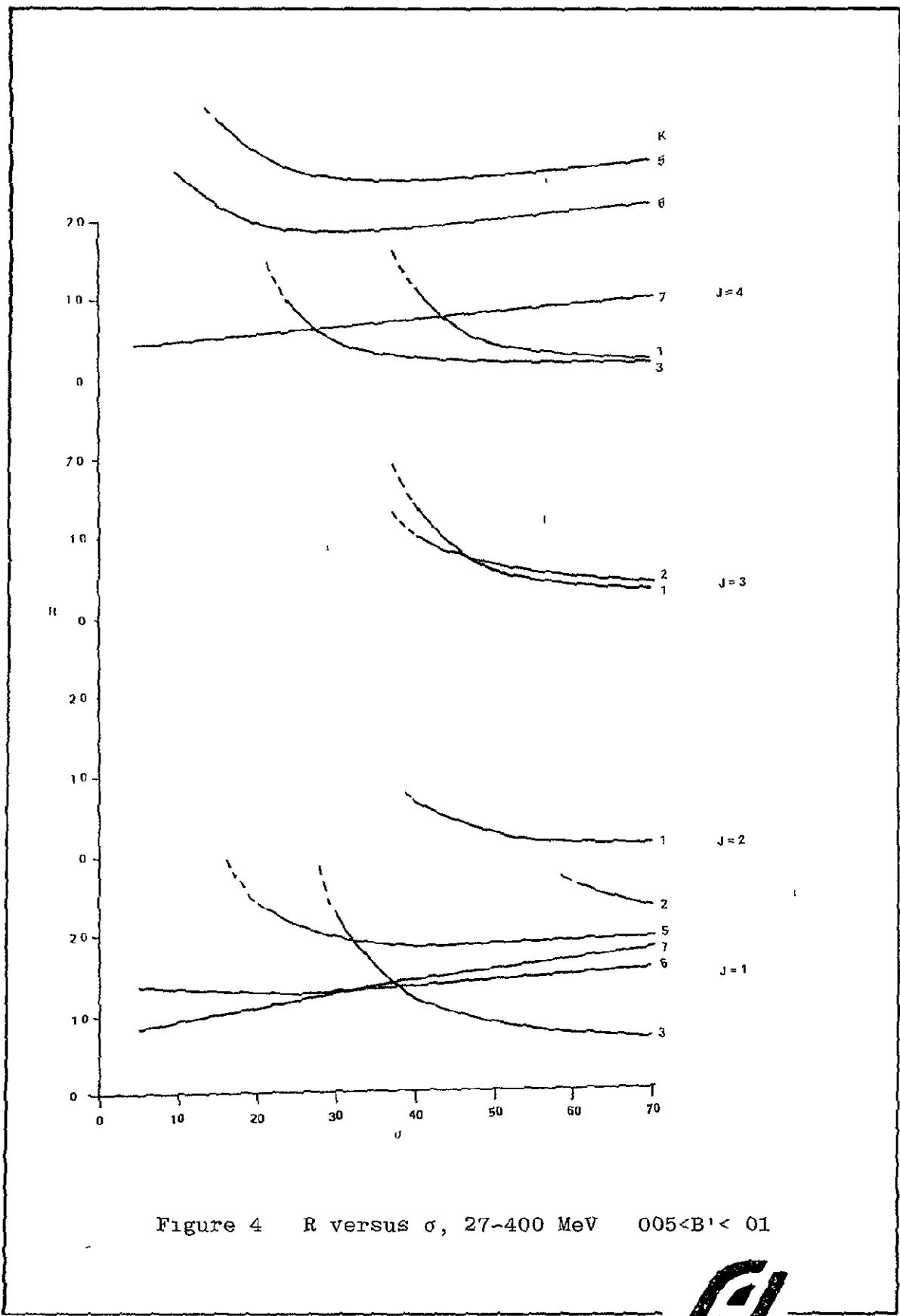


Figure 4 R versus σ , 27~400 MeV $0.05 < B' < 0.1$

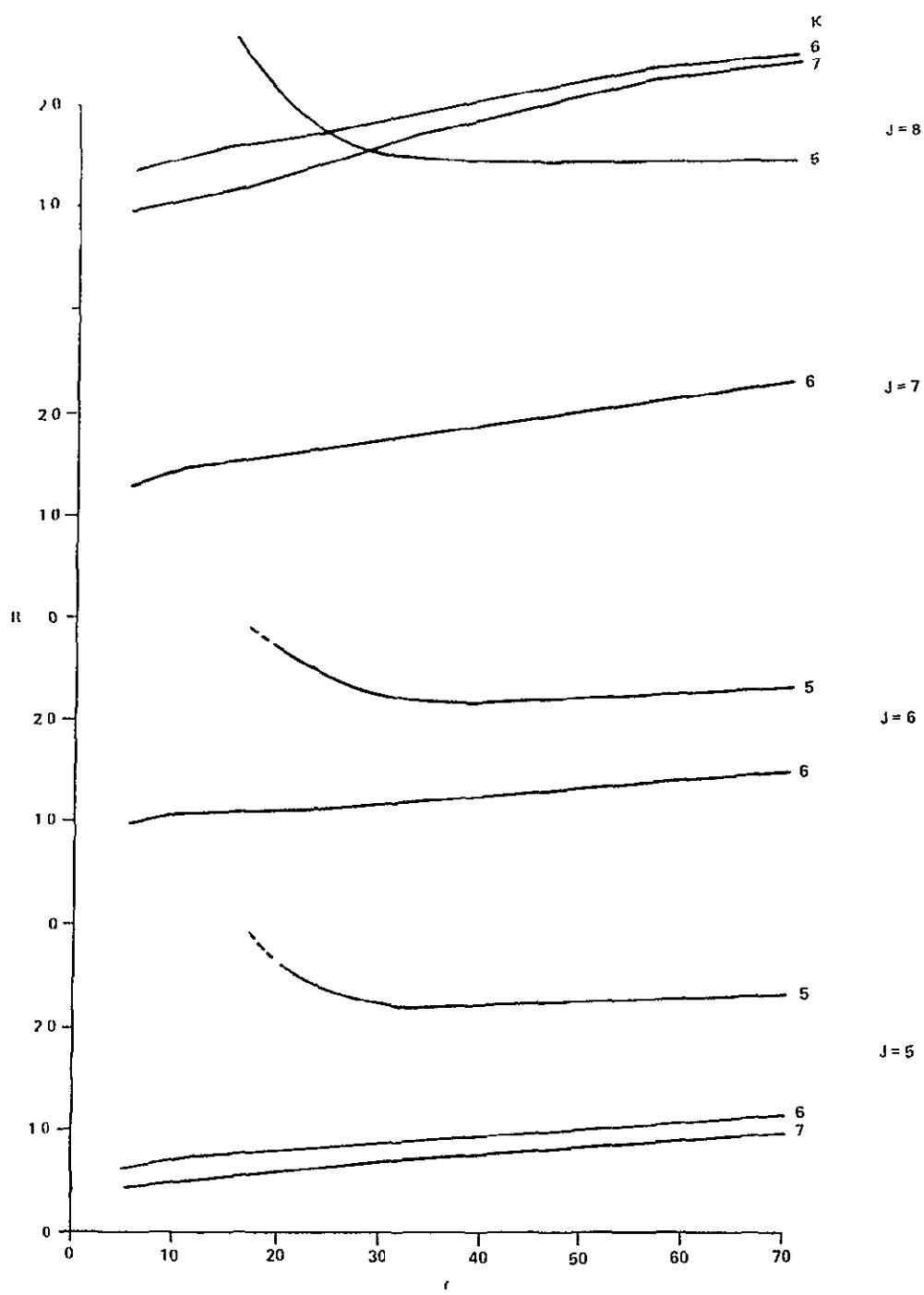


Figure 4 Continued

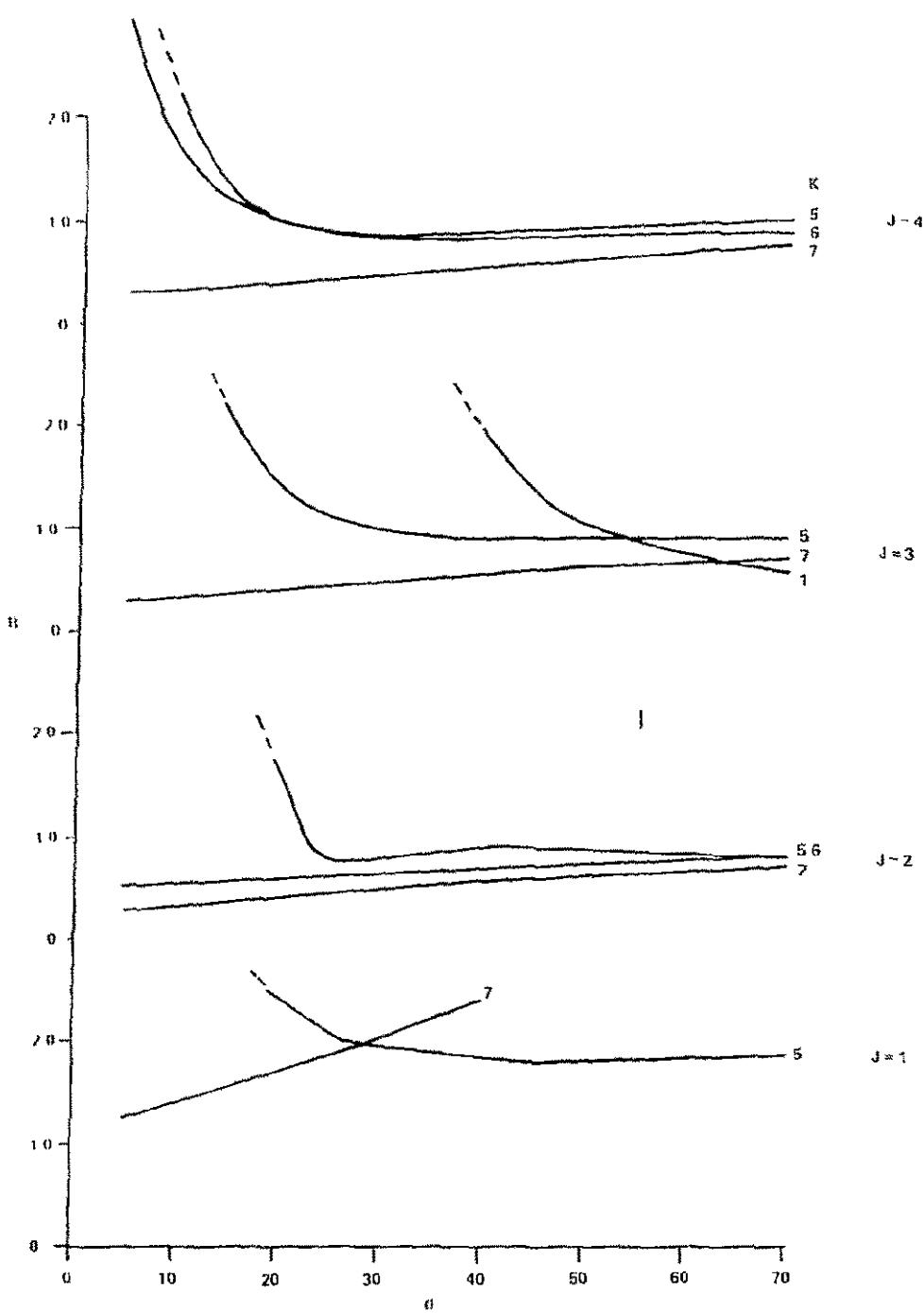


Figure 5 R versus σ , 27-400 MeV $01 < B' < 02$

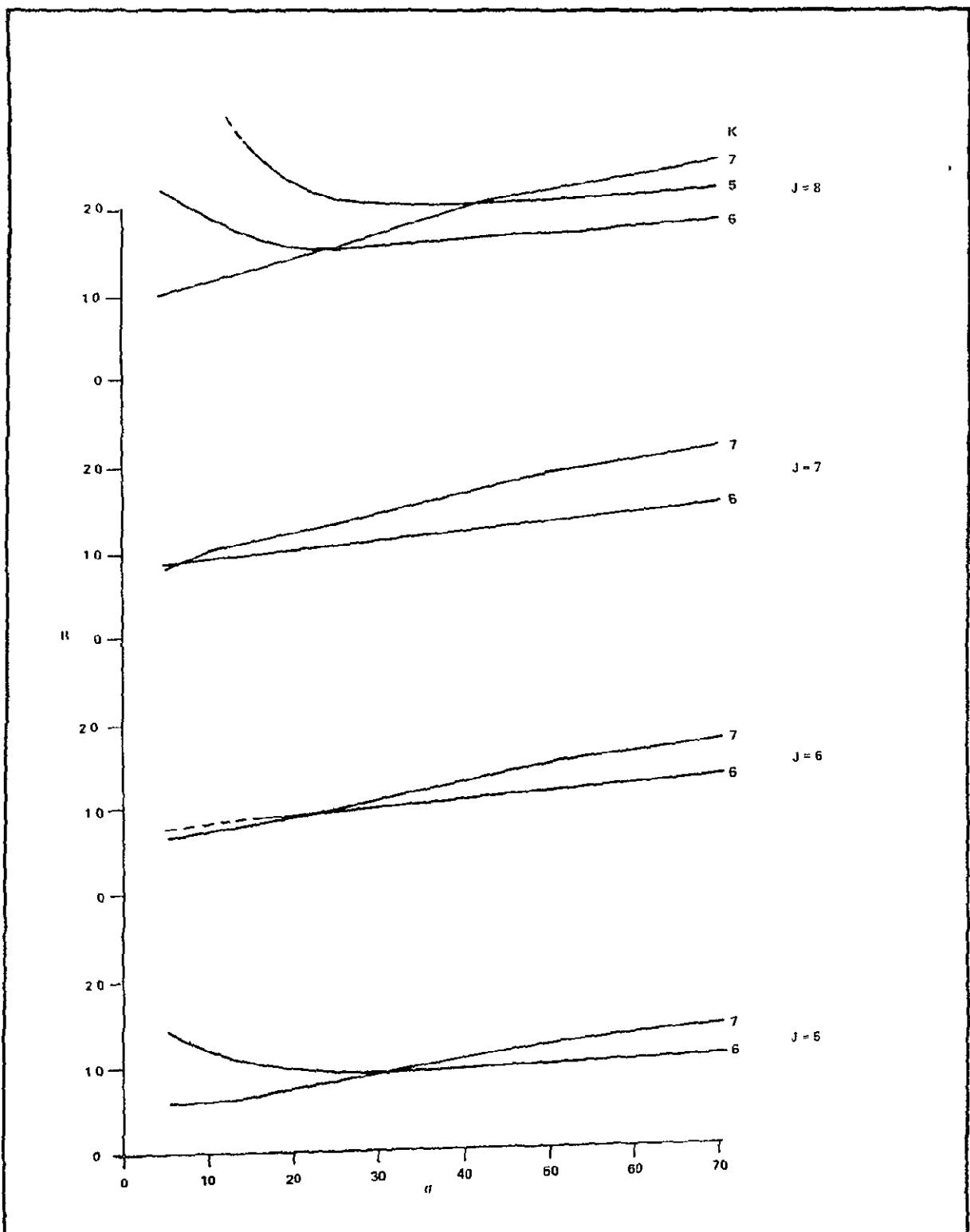


Figure 5 Continued

plot of R, the measured flux divided by the model flux, versus σ for I=1 ($0 < B' < 005$) Figures 4 and 5 are for I=2 ($005 < B' < 01$) and I=3 ($01 < B' < 02$) Eight plots are shown in the figure, one for each L' band labeled J=1-8 These I, J bands may be correlated with the dashed boxes of Figure 2, which was constructed with the AP7 model rather than the AP3 model used herein Within each plot the curves are labeled by the index K A value of K equal to 1 identifies measurements taken when the spectrometer view axis is within 30 degrees of the field line, either parallel or antiparallel K=2 corresponds to 30° to 40° look angles, etc , up to K=7 where the look angle is within 10° of perpendicularity and maximum count rates should occur

The K=7 curves increase monotonically with σ because the model flux (denominator of R) is decreasing The K=6 curves exhibit similar behavior for large σ , but may show a slight rise at small σ For K=1 to 5, the value of R is very large at small values of σ because the model flux is small at these angles

The curves of Figures 3, 4, and 5 show that σ should be at least 40° to 50° in the 27 to 400 MeV range in order for the model flux to simulate the measurements at small angles to the field lines

Figures 6-8 show similar curves for the low energy group, 18 to 27 MeV The absolute values of the ratio, R, are less significant because the AP3 model is not valid down to 18 MeV However, the relative magnitudes of the K=1, 2 versus K=7 curves show that a σ value of 70° or larger is necessary to permit the model flux to simulate the measurements in the low energy range

The angular distribution of the trapped protons should be energy dependent at 235 nautical miles altitude, because of the scavenging effect of the atmosphere Higher energy protons must have a smaller value of σ in the SA anomaly as



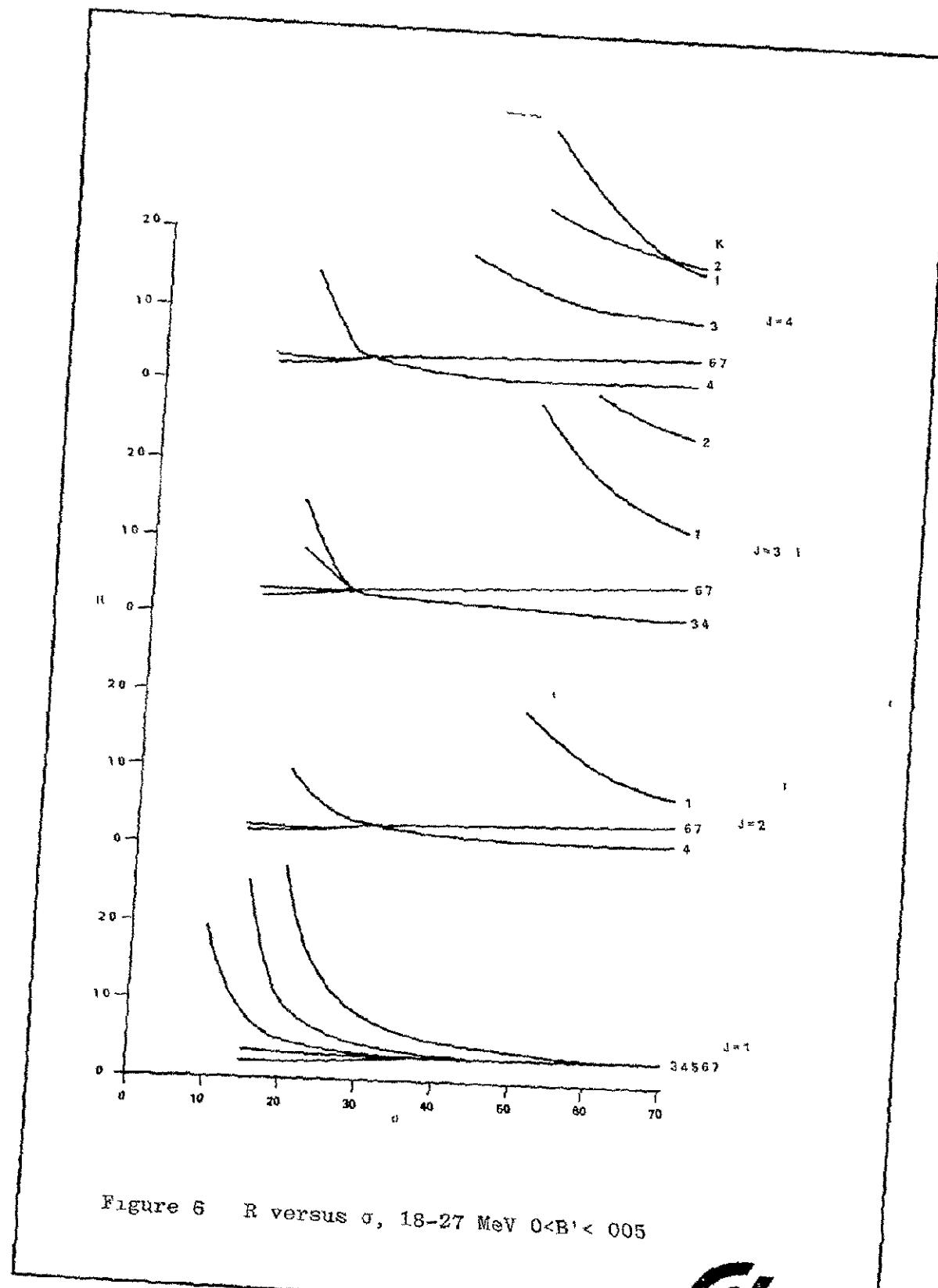


Figure 6 R versus σ , 18-27 MeV $0 < B' < 0.05$

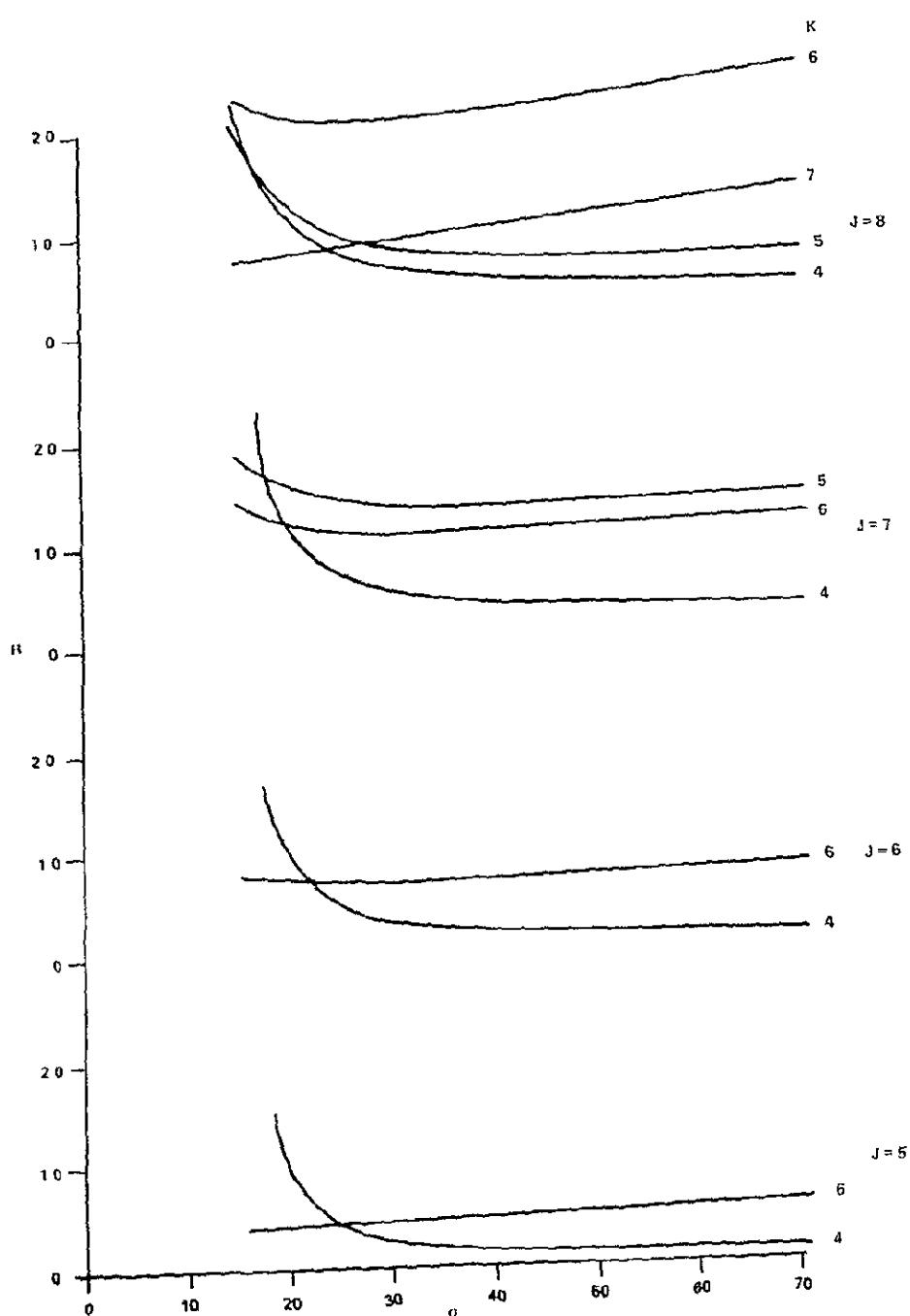


Figure 6 Continued

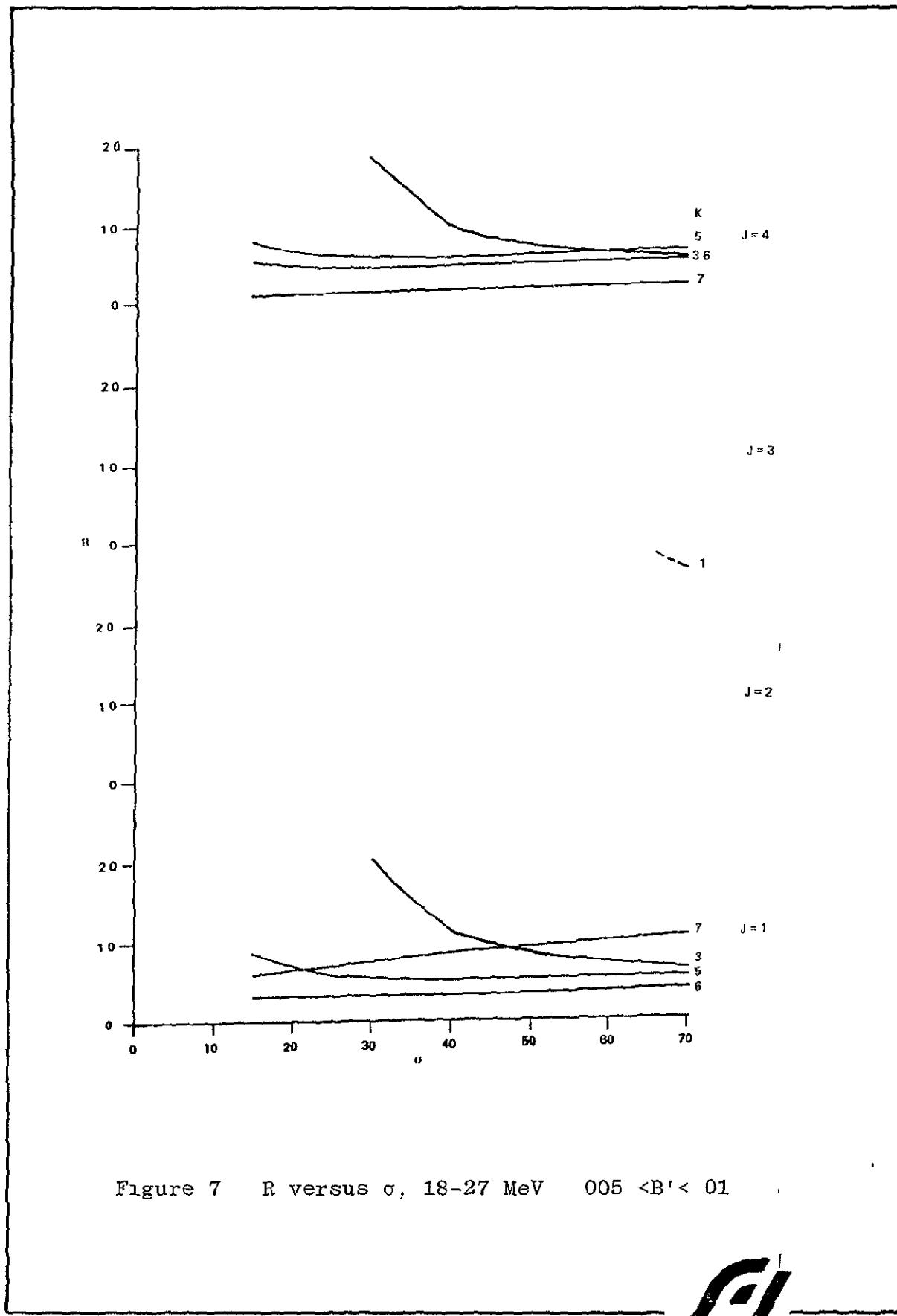


Figure 7 R versus σ , 18-27 MeV $005 < B' < 01$

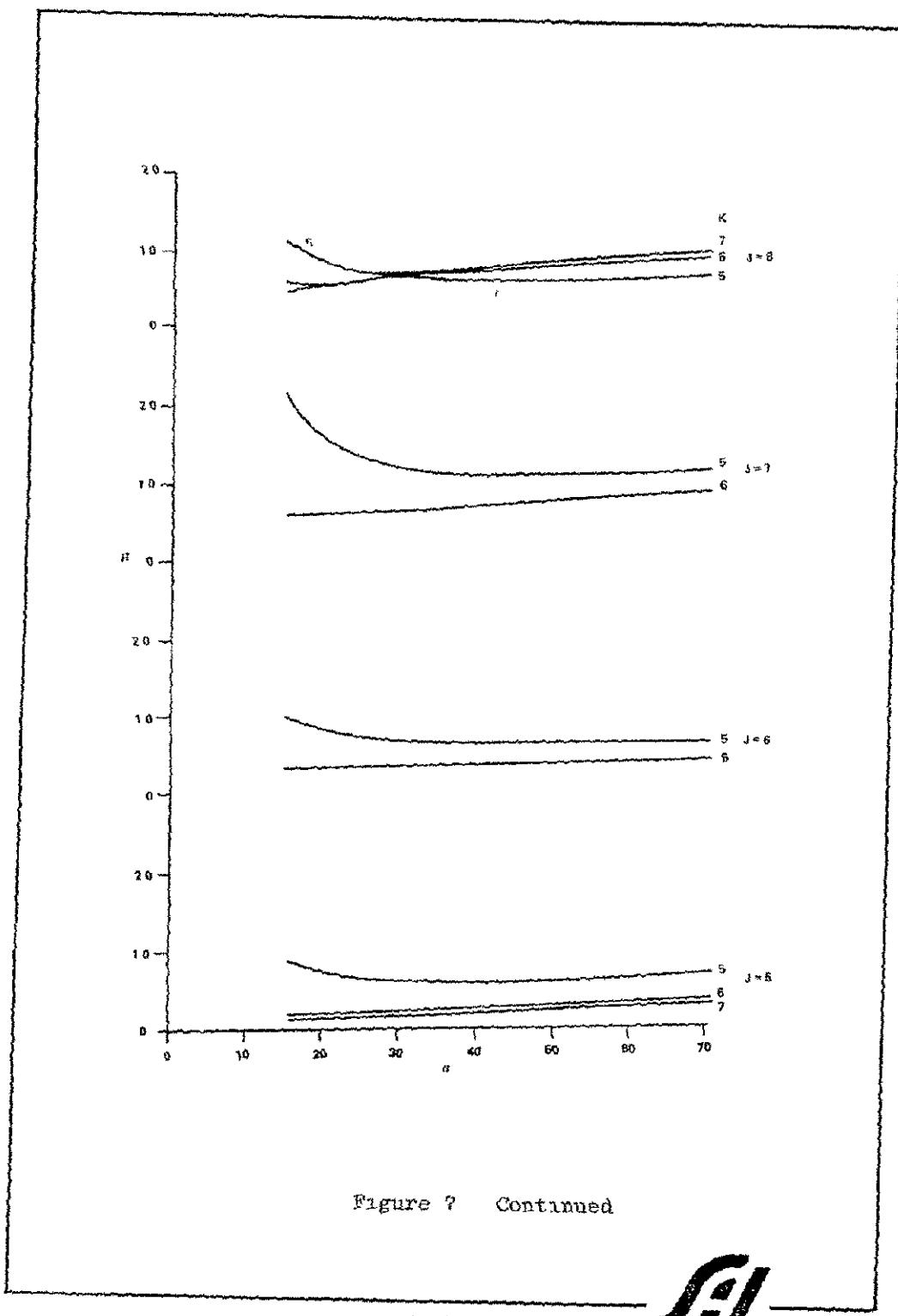


Figure ? Continued

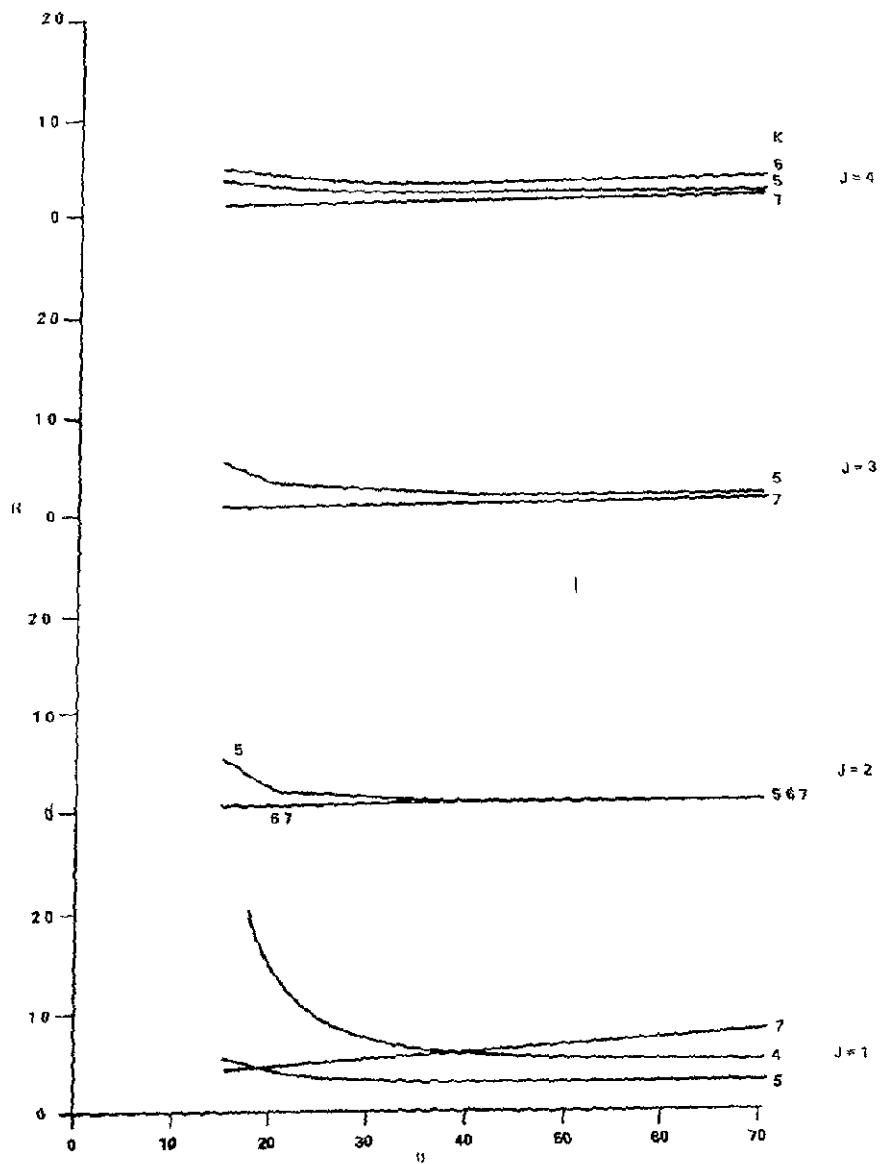


Figure 8 R versus σ , 18-27 MeV $01 < B' < 02$

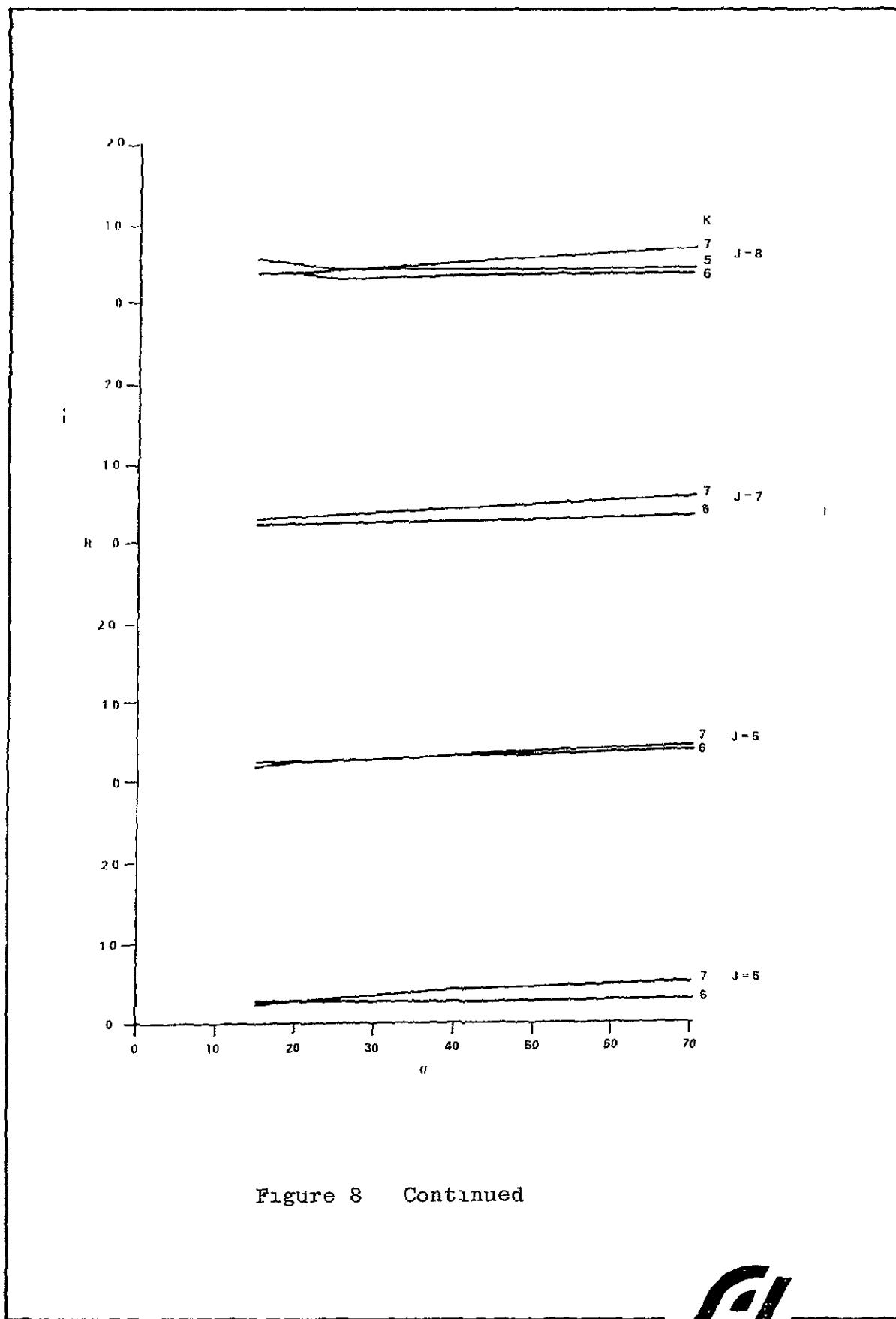


Figure 8 Continued

they approach their mirror point than the lower energy protons possess

It is unfortunate that the loss of spectral information prevents a better study of pitch angle versus energy

Within each B' , L' box, the ratio of experimental to model counts has been summed over pitch angle, using weights determined from model f sd's The results are presented in Figures 9-11 Figure 9 is for the lower B' values, Figure 10 is for the middle B' values, and Figure 11 is for the higher B' values observed The top graph in each figure pertains to the 18-27 MeV band, the bottom graph, to the 27-400 MeV band Each curve is labeled by its L' band

These figures must be interpreted carefully because some pitch angle bands are empty Dashed lines indicate that some ratios have exceeded program constraints

The low energy curves of Figures 9-11 are systematically small except for the top 3 L' bands for lowest B' At large values of σ , the AP3 model-extrapolated down to 18 MeV-generally predicts more counts than the experiment measures by a factor of 2 to 5 The top three curves of Figure 9 show good agreement between experiment and the model in this region

The high energy curves of Figures 9-11 should be interpreted at values of σ between 40° and 60° The curves are probably most valid for the low portion of the 27 to 400 MeV energy range where most of the flux exists The ratio of measured to model counts is large for L' bands 1, 7, and 8 The ratio is smaller for L' bands 2, 3, and 4 It would appear that the model fluxes are too low near the top and bottom of Figure 2

The east-west asymmetry data of Table A-3 are not amenable to analysis because of insufficient data



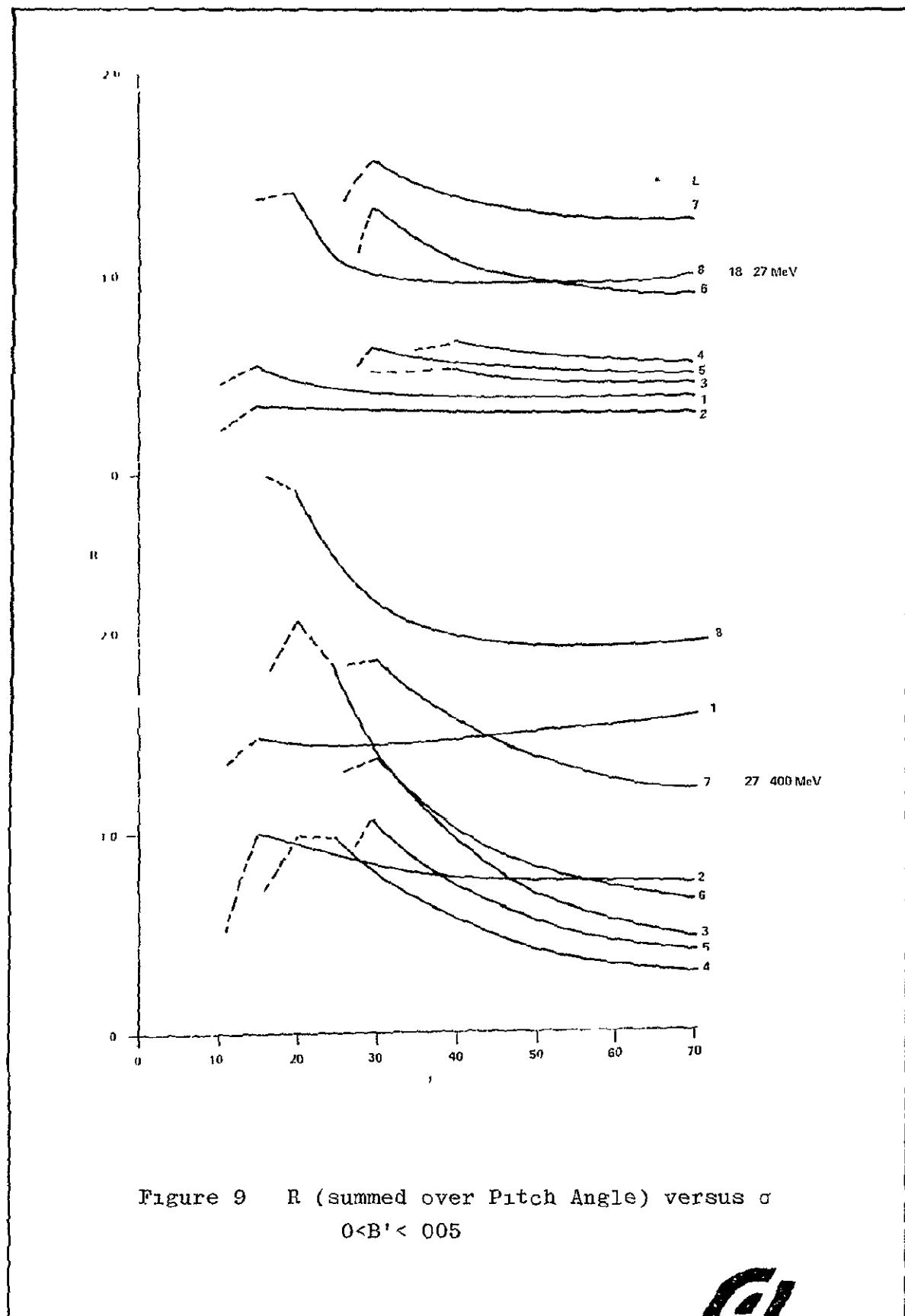


Figure 9 R (summed over Pitch Angle) versus σ
 $0 < B' < 005$

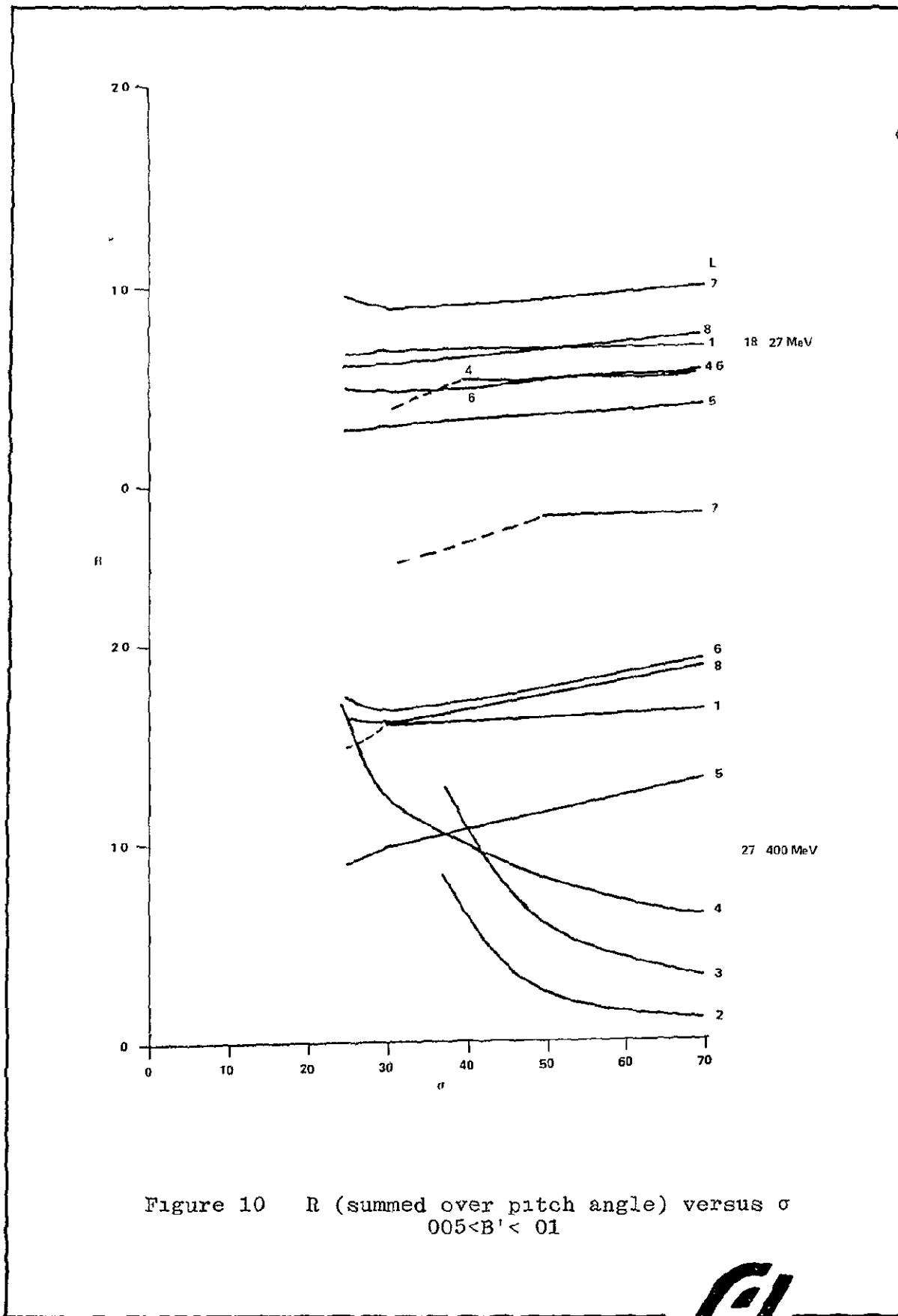


Figure 10 R (summed over pitch angle) versus σ
 $0.05 < B' < 0.1$

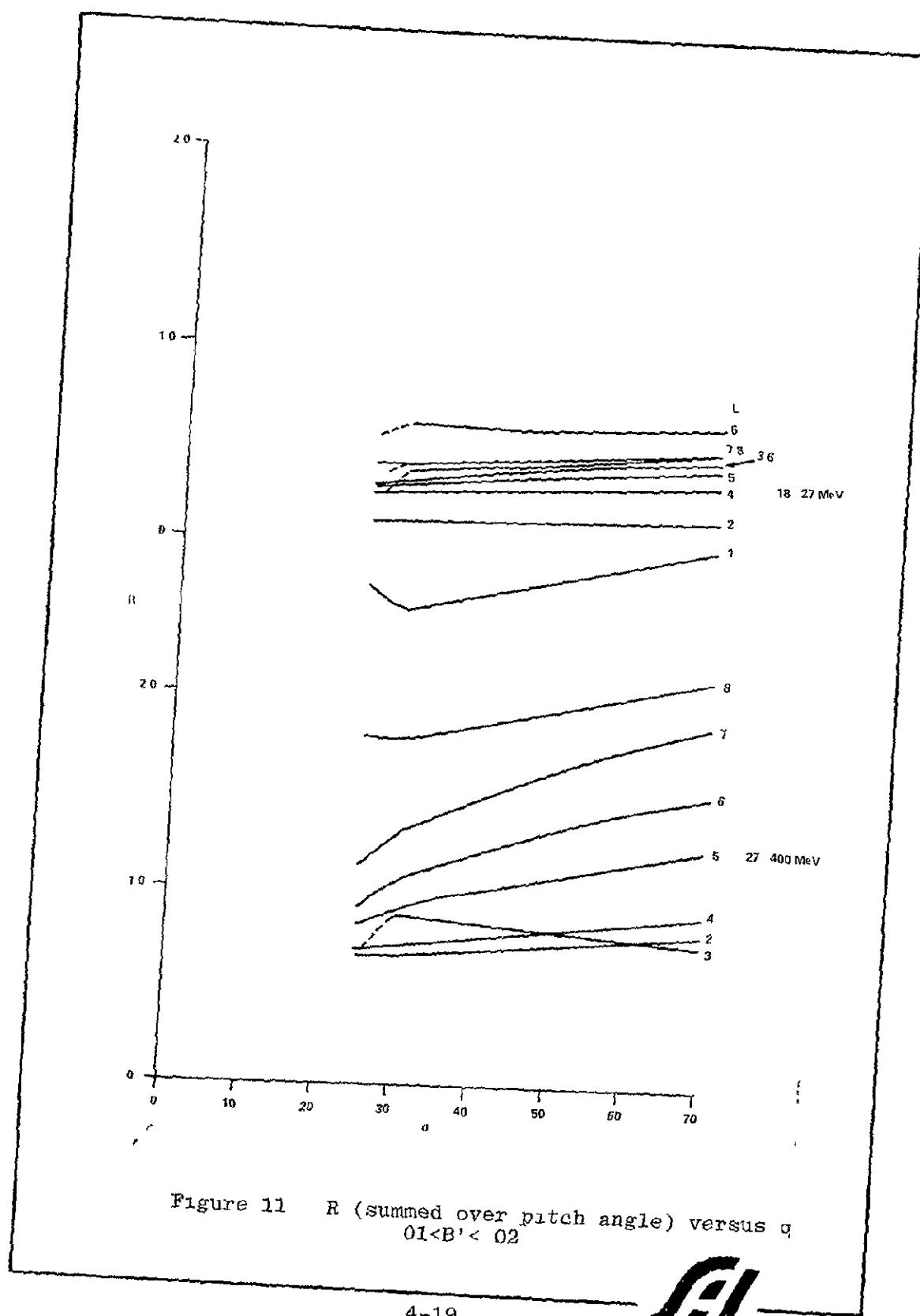


Figure 11 R (summed over pitch angle) versus q
 $01 < B' < 02$

5 REFERENCES

- 1 Operations Handbook for the Proton Spectrometer, NASA Contract NAS8-26215, Document #CD105070-3, Spacetac, Inc, May 17, 1971
2. Gary R Streeter, G A Guenther, A Digital Closed Loop Calibration System for Space-Borne Particle Spectrometers, Proceedings of IEEE, Vol NS16, pp 124-9, 15th Nuclear Science Symposium, San Francisco, October 1969
- 3 J. I. Vette, et al., Models of the Trapped Radiation Environment, Vols I-VI, NASA SP-3024, 1966-1970



Table A1 Ratio of Measured to Model Counts as a
Function of B' , L' , and α



REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR.

BIN RATIOS H = 1			R	FSD1	PFS01	R	FSD1	PFS01	R	FSD1	PFS01
I	J	K NO									
1	1	3 7		.00000	.000	.866	.00000	.000	1.296	.00000	.000
1	1	4 87		.00000	.000	.760	.00000	.000	1.021	.00000	.000
1	1	5 126	16.97762	3.110	.455	85.33444	2.499	.646	82.14015	3.170	.592
1	1	6 40	.44750	.675	.956	1.57181	.561	.770	1.53122	1.082	.627
1	1	7 51	.16214	.165	.770	.86458	.163	.178	.71171	.164	.177
1	2	1 1	.00000	.000	.000	.00000	.000	.000	.00000	.000	.000
1	2	4 98	.00000	.000	.471	.00000	.000	.220	.00000	.000	.215
1	2	6 37	.23632	.228	.513	.47794	.229	.494	.72215	.229	.323
1	2	7 134	.17170	.159	.492	.73280	.404	.548	.64442	.470	.560
1	3	1 32	.00000	.000	.341	.00000	.000	.530	.00000	.000	.275
1	3	2 77	.10000	.000	.265	.00000	.000	.353	.00000	.000	.194
1	3	3 44	.00000	.000	.745	.00000	.000	.263	.00000	.000	.252
1	3	4 26	.00000	.000	.865	.00000	.000	.220	.00000	.000	.210
1	3	6 44	.27495	.734	.369	.17616	.072	.109	.97093	.064	.105
1	3	7 92	.19330	.171	.370	.64954	.587	1.135	.70675	.818	.955
1	4	1 31	.00000	.000	.353	.00000	.000	.397	.00000	.000	.305
1	4	2 18	.00000	.000	.284	.00000	.000	.339	.00000	.000	.237
1	4	3 11	.00000	.000	.494	.00000	.000	.610	.00000	.000	.348
1	4	4 53	.00000	.000	.796	.00000	.000	.297	.00000	.000	.264
1	4	6 16	.31660	.311	.377	.146498	.286	.359	.12210	.349	.350
1	4	7 46	.20493	.011	.398	.28600	.120	.301	.73918	.041	.208
1	5	1 28	.00000	.000	.385	.00000	.000	.484	.00000	.000	.359
A1	5	4 49	.00000	.000	1.057	.00000	.000	.264	.00000	.000	.273
A1	5	6 14	.33400	.087	.333	.46437	.121	.419	.15664	.153	.178
A1	6	1 25	.00000	.000	.149	.00000	.000	.541	.00000	.000	.150
A1	6	4 44	.00000	.000	.593	.00000	.000	.291	.00000	.000	.269
A1	6	6 12	1.06844	.322	.356	1.53793	.377	.357	3.09246	.424	.287
A1	7	1 4	.00000	.000	.214	.00000	.000	.512	.00000	.000	.186
A1	7	4 41	.00000	.000	.495	.00000	.000	.283	.00000	.000	.227
A1	7	5 6	10.19455	.271	.266	13.17623	.281	.204	43.35653	.290	.266
A1	7	6 10	3.07637	.179	.364	4.08708	.201	.330	9.57178	.221	.302
A1	8	4 20	.00000	.000	.477	.00000	.000	.379	.00000	.000	.294
A1	8	5 89	316.59642	5.586	.406	953.96806	5.578	.420	517.10471	5.583	.282
A1	8	6 14	2.76653	.456	.360	3.60945	.484	.544	3.13829	.464	.131
A1	8	7 149	.58440	.414	.400	1.21149	.553	.668	.82896	.471	.470
2	1	2 6	.00000	.000	.610	.00000	.000	1.077	.00000	.000	.769
2	1	3 25	.00000	.000	1.217	.00000	.000	1.247	.00000	.000	1.025
2	1	5 27	9.40238	1.750	1.000	34.15017	1.748	.309	30.04924	1.748	.310
2	1	6 46	.32095	.333	1.402	1.31564	.345	.399	1.11870	.343	.395
2	1	7 7	.46858	.132	.745	.80540	.126	.236	.4146	.127	.158
2	2	1 7	.00000	.000	.222	.00000	.000	.544	.00000	.000	.149
2	3	1 25	.00000	.000	.273	.00000	.000	.682	.00000	.000	.206
2	3	2 57	.00000	.000	.253	.00000	.000	.365	.00000	.000	.206
2	4	1 18	.00000	.000	.765	.00000	.000	.439	.00000	.000	.239
2	4	3 13	.00000	.000	.414	.00000	.000	.298	.00000	.000	.245
2	4	5 4	2.54610	.102	.265	11.12411	.112	.062	8.56820	.109	.081
2	4	6 74	.85947	.378	.419	3.40052	.428	.096	2.72374	.414	.092
2	4	7 6	.08209	.004	.470	.34917	.004	.210	.31132	.002	.191
2	5	5 35	10.04703	.827	.143	33.96453	.855	.161	26.61374	.846	.149
2	5	6 28	.17668	.024	.448	.61196	.077	.195	.46398	.059	.190
2	5	7 18	.11489	.018	.473	.41654	.021	.179	.32818	.009	.155
2	6	5 12	.00000	.000	.399	.00000	.000	.125	.00000	.000	.128
2	6	6 51	.28911	.122	.403	.98089	.186	.190	.70273	.153	.168
2	7	5 15	.00000	.000	.239	.00000	.000	.179	.00000	.000	.122

2	7	6	28	.45363	.039	.421	1.27298	.139	.198	.85894	.089	.180
2	8	5	11	.00000	.000	.484	.00000	.000	.380	.00000	.000	.127
2	8	6	40	.42664	.463	.465	1.31767	.609	.834	.80294	.524	.733
2	8	7	02	.36364	.217	.510	.98238	.338	.505	.61422	.253	.413
3	1	2	2	.00000	.000	.000	.00000	.000	.000	.00000	.000	.333
3	1	4	5	.10000	.000	.000	.00000	.000	.128	.01626	.000	.144
3	1	5	22	8.08522	2.126	1.972	49.24559	2.122	.194	41.37499	2.122	.191
3	1	7	3	.32677	.133	.414	1.20680	.128	.062	1.019229	.129	.060
3	2	5	75	35.58767	6.054	1.764	264.76329	6.055	.303	221.16704	6.054	.309
3	2	6	49	.07000	.598	1.982	.53878	.606	.275	.45446	.604	.271
3	2	7	41	.04904	.362	1.424	.30791	.313	.351	.26156	.320	.331
3	3	1	54	.00000	.000	.386	.00000	.000	.424	.00000	.000	.325
3	3	4	84	.00000	.010	1.023	.00000	.000	.266	.00000	.000	.266
3	3	2	119	.06476	.378	1.180	.29183	.314	.325	.24611	.324	.322
3	4	5	58	4.41253	1.611	.919	17.41717	1.596	.234	14.06613	1.600	.231
3	4	6	11	1.13546	.125	.342	2.96573	.112	.211	2.47522	.115	.197
3	4	7	52	.08793	.073	.475	.31527	.043	.236	.25907	.039	.223
3	5	6	56	.36780	.333	.546	1.37121	.246	.207	1.016084	.273	.204
3	5	7	18	.20271	.004	.516	.56631	.026	.207	.45149	.016	.173
3	6	6	52	.22818	.038	.597	.74151	.080	.251	.55564	.036	.226
3	6	7	37	.18484	.014	.511	.65614	.105	.261	.49256	.069	.243
3	7	6	24	.18601	.343	.943	.86735	.463	.524	.51435	.406	.524
3	7	7	86	.23711	.057	.524	.88213	.154	.270	.56783	.104	.231
3	8	5	8	1.07020	.345	.622	15.70474	.349	.189	8.40211	.347	.261
3	8	6	33	.47889	.454	.748	2.21216	.546	.354	1.26136	.498	.274
3	8	7	85	.27484	.107	.545	1.03397	.154	.354	.61274	.124	.299
4	7	6	2	.00000	.000	.000	.57345	.005	.000	.31873	.003	.000

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

BIN RATIOS H= 2												
I	J	K	NO	R	FSDI	PFSDI	R	FSDI	PFSDI	R	FSDI	PFSDI
1	1	3	7	.00000	.000	.866	.00000	.000	1.296	.00000	.000	.980
1	1	4	87	42.13157	2.622	.706	141.15185	2.983	1.021	128.34590	3.058	.880
1	1	5	26	1.88954	1.0046	.855	8.71263	1.049	.696	8.17903	1.131	.542
1	1	6	60	.41312	.547	.946	1.39316	.684	.770	1.37758	.818	.627
1	1	7	51	.17979	.174	.770	.46096	.171	.178	.78922	.172	.177
1	2	1	1	.00000	.000	.000	.00000	.000	.000	.00000	.000	.000
1	2	4	98	.00000	.000	.671	.00000	.000	.220	.00000	.000	.215
1	2	6	37	.26425	.210	.513	.31080	.211	.444	.80750	.212	.323
1	2	7	34	.18773	.160	.492	.79784	.405	.548	.70110	.470	.500
1	3	1	32	.00000	.000	.341	.60000	.087	.530	.00000	.000	.275
1	3	2	77	.00000	.000	.208	.60000	.000	.353	.00000	.000	.194
1	3	3	44	.00000	.000	.745	.00000	.000	.263	.00000	.000	.252
1	3	4	26	.00000	.000	.865	.00000	.000	.220	.00000	.000	.210
1	3	6	44	.31002	.043	.369	1.32583	.080	.169	1.029455	.071	.105
1	3	7	97	.21095	.164	.370	.71860	.667	1.135	.78521	.801	.955
1	4	1	30	.00000	.017	.253	.00000	.001	.397	.00000	.000	.305
1	4	2	14	.00000	.000	.284	.60000	.000	.339	.00000	.000	.237
1	4	3	11	.00000	.000	.494	.60000	.000	.610	.00000	.000	.348
1	4	4	53	.00000	.000	.796	.60000	.000	.297	.00000	.000	.264
1	4	6	16	.33894	.263	.377	1.56143	.237	.359	1.29671	.307	.350
1	4	7	46	.22805	.011	.398	.31819	.030	.361	.82216	.051	.208
1	5	1	28	.00000	.010	.385	.00000	.000	.484	.00000	.000	.359
1	5	4	49	.70000	.000	1.057	.60000	.000	.264	.00000	.000	.273
1	5	6	14	.37877	.096	.333	.52645	.124	.419	1.31084	.161	.178
1	6	1	29	.00000	.000	.149	.00000	.000	.541	.00000	.000	.150
1	6	4	44	.70000	.010	.593	.00001	.000	.291	.00000	.000	.269
1	6	6	12	.91121	.225	.356	1.31846	.281	.357	2.66425	.333	.287
1	7	1	4	.00000	.000	.214	.00000	.000	.512	.00000	.000	.166
1	7	4	41	.00000	.000	.595	.00000	.000	.283	.00000	.000	.227
1	7	5	6	2.73071	.064	.266	3.53545	.074	.204	11.65803	.085	.266
1	7	6	10	1.86235	.102	.169	2.48363	.125	.330	5.82674	.146	.302
1	8	4	20	18.27202	1.025	.527	59.09650	1.019	.379	36.44242	1.022	.294
1	8	5	89	7.09079	1.243	.406	19.67220	1.074	.420	13.66859	.999	.282
1	8	6	14	2.50824	.334	.386	3.24856	.380	.544	2.74814	.348	.131
1	8	7	149	.64525	.407	.400	1.34621	.540	.668	.91596	.458	.470
2	1	2	-6	.00000	.000	.000	.00000	.000	1.077	.00000	.000	.769
2	1	3	25	.00000	.000	1.317	.00100	.000	1.247	.00000	.000	1.025
2	1	5	27	1.49997	.687	1.000	5.42115	.677	.304	4.64152	.679	.310
2	1	6	46	.32457	.196	1.462	1.33610	.204	.399	1.013516	.202	.395
2	1	7	7	.52528	.125	.745	.90281	.118	.236	.83115	.120	.158
2	2	1	7	.00000	.000	.222	.00000	.000	.544	.00000	.000	.149
2	3	1	25	.00000	.000	.273	.00000	.000	.602	.00000	.000	.286
2	3	2	57	.00000	.000	.253	.00000	.000	.365	.00000	.000	.206
2	4	1	18	.00000	.000	.265	.00000	.000	.439	.00000	.000	.239
2	4	3	13	.00000	.000	.411	.00000	.000	.298	.00000	.000	.245
2	4	5	4	1.03699	.029	.365	4.49313	.034	.064	3.49146	.034	.081
2	4	6	34	.64421	.203	.409	2.57197	.255	.098	2.05512	.241	.092
2	4	7	6	.09116	.004	.500	.44325	.006	.210	.34571	.003	.191
2	5	5	35	1.34139	.079	.343	4.83764	.169	.161	3.71288	.140	.149
2	5	6	28	.19173	.028	.448	.08726	.081	.195	.52110	.064	.190
2	5	7	18	.12924	.013	.473	.47071	.025	.179	.36911	.014	.155
2	6	5	12	1.53859	.010	.399	5.28116	.035	.125	3.89131	.026	.128
2	6	6	51	.32102	.065	.403	1.00852	.155	.190	.78001	.114	.168
2	7	5	15	5.84274	.080	.239	19.31145	.127	.179	12.04366	.104	.122

2	7	6	2H	.51185	.034	.421	1.43711	.133	.198	.96943	.043	.180	
2	8	5	11	2.22786	.245	.484	5.72109	.267	.380	3.06091	.254	.127	
2	8	6	40	.47838	.467	.465	1.47579	.613	.834	.90006	.529	.733	
2	8	7102		.39531	.218	.510	1.06794	.306	.505	.66766	.253	.413	
3	1	2	2	.00000	.000	.000	.00000	.000	.000	.00000	.000	.333	
3	1	4	5	.00000	.000	2.000	.00000	.000	.128	.00000	.000	.104	
3	1	5	22	1.044949	.932	1.972	6.47069	.940	.194	5.42640	.939	.191	
3	1	7	3	.35904	.132	1.414	1.39189	.127	.083	1.20015	.128	.000	
3	2	5	75	14.98534	4.043	1.764	11.49125	4.043	.303	93.13236	6.043	.309	
3	2	6	49	.07500	.517	1.982	.57832	.527	.275	.48765	.525	.271	
3	2	7	41	.05467	.346	1.424	.34318	.305	.351	.29154	.312	.131	
3	3	1	54	.00000	.000	.186	.00000	.000	.424	.00000	.000	.325	
3	3	5	84	1.99150	.657	1.023	8.58442	.642	.266	7.25888	.646	.266	
3	3	7114		.07034	.390	1.180	.31614	.324	.326	.26747	.317	.322	
3	4	5	58	.62220	.401	.919	2.29472	.338	.234	1.88511	.354	.231	
3	4	6	11	.61885	.062	.142	1.61482	.639	.211	1.34809	.043	.197	
3	4	7	52	.09630	.065	.475	.34607	.043	.236	.28360	.034	.223	
3	5	6	56	.31216	.206	.546	1.15n32	.116	.207	.89315	.143	.204	
3	5	7	18	.21621	.008	.516	.00405	.024	.207	.48156	.014	.173	
3	6	6	57	.25866	.047	.597	.06414	.071	.251	.63029	.027	.226	
3	4	7	37	.19763	.020	.411	.73320	.111	.261	.52647	.074	.243	
3	7	6	24	.20994	.351	.993	.91007	.474	.529	.58014	.417	.524	
3	7	7	84	.26253	.060	.524	.97A63	.157	.270	.62868	.108	.231	
3	8	5	8	.79328	.058	.422	4.06334	.063	.189	2.17219	.080	.261	
3	8	6	33	.4n627	.238	.748	1.90318	.316	.354	1.07685	.273	.274	
3	8	7	85	.3n366	.113	.545	1.14198	.160	.354	.67689	.132	.299	
A	4	7	6	2	.00000	.001	.000	.64108	.005	.000	.35676	.003	.000

CR

BIN RATIOS M= 3												
I	J	K	NO	R	F501	PFS01	R	F501	PFS01	R	F501	PFS01
1	1	3	7	34.03313	1.584	.866	90.98918	1.583	1.296	122.40067	1.583	.980
1	1	4	87	2.52062	.800	.766	8.54070	1.071	1.021	7.82534	1.120	.880
1	1	4	124	.76394	.478	.855	3.30288	.534	.696	3.04678	.619	.592
1	1	4	60	.36054	.514	.456	1.25940	.539	.770	1.25567	.674	.627
1	1	7	51	.19931	.100	.770	1.06632	.178	.178	.87492	.178	.177
1	2	1	1	.00000	.010	.000	.00000	.000	.000	.00000	.000	.000
1	2	4	98	7.39703	1.434	.671	36.40761	1.437	.220	29.90639	1.437	.215
1	2	4	17	.27726	.185	.513	.32611	.186	.494	.84728	.186	.323
1	2	7	134	.20683	.147	.492	.57726	.406	.540	.77064	.470	.500
1	3	1	32	.00000	.000	.341	.00000	.000	.530	.00000	.000	.275
1	3	2	77	.00000	.000	.208	.00000	.000	.353	.00000	.000	.194
1	3	3	44	3.54961	.021	.745	14.23406	.329	.763	11.72756	.022	.252
1	3	4	26	.00000	.000	.805	.00000	.000	.220	.00000	.000	.210
1	3	6	44	.32931	.025	.369	.140479	.071	.109	.1.16296	.043	.165
1	3	7	97	.23218	.191	.370	.79639	.557	.1.135	.87209	.792	.955
1	4	1	30	.00000	.000	.353	.00000	.001	.397	.00000	.000	.305
1	4	2	14	.00000	.000	.284	.00000	.000	.339	.00000	.000	.237
1	4	3	01	388.14504	3.479	.494	69.14958	1.779	.610	149.44047	3.979	.348
1	4	4	53	.00000	.000	.796	.00000	.000	.297	.00000	.000	.264
1	4	6	16	.34242	.204	.377	1.56193	.230	.359	1.29417	.300	.350
1	4	7	46	.25372	.014	.398	.35396	.034	.301	.91452	.054	.208
1	5	1	28	.00000	.000	.385	.00000	.000	.484	.00000	.000	.359
1	5	4	49	7.23760	1.349	1.057	31.50977	1.337	.264	22.86299	1.341	.273
A1	1	5	6	.39958	.044	.233	.56458	.119	.419	1.38391	.151	.178
1	6	1	29	.00000	.000	.149	.00000	.000	.541	.00000	.000	.150
1	6	4	44	4.89449	.889	.493	13.96195	.925	.291	10.27851	.909	.269
1	6	6	12	.80870	.170	.356	1.17366	.225	.357	2.37839	.279	.287
1	7	1	4	.00000	.000	.214	.00000	.000	.512	.00000	.000	.186
1	7	4	41	3.054875	.193	.695	9.25910	.102	.283	6.12911	.148	.227
1	7	5	6	1.88415	.041	.266	2.43998	.052	.204	8.04761	.042	.266
1	7	6	10	1.41884	.075	.369	1.89339	.098	.330	4.44472	.120	.302
1	8	4	20	2.27462	.315	.577	7.04983	.340	.379	4.39138	.326	.294
1	8	5	89	2.08176	.447	.606	5.31487	.302	.420	3.55966	.303	.282
1	8	6	14	2.29063	.294	.386	2.95587	.349	.544	2.50670	.311	.131
1	8	7	149	.71443	.401	.410	1.48436	.534	.666	1.01454	.442	.470
2	1	2	6	.00000	.000	.000	.00000	.000	1.077	.00000	.000	.769
2	1	3	25	.00000	.000	.1317	.00000	.000	1.247	.00000	.000	1.025
2	1	5	27	.86428	.444	1.000	3.07427	.430	.309	2.63509	.432	.310
2	1	6	46	.31498	.148	1.402	1.30031	.142	.399	1.10412	.143	.395
2	1	7	7	.58620	.122	.745	1.00750	.116	.236	.92754	.117	.158
2	2	1	7	.00000	.000	.222	.00000	.000	.544	.00000	.000	.149
2	3	1	25	.00000	.000	.273	.00000	.000	.682	.00000	.000	.286
2	3	2	57	.00000	.000	.253	.00000	.000	.365	.00000	.000	.206
2	4	1	18	.00000	.000	.265	.00000	.000	.439	.00000	.000	.239
2	4	3	13	.00000	.000	.410	.00000	.000	.298	.00000	.000	.245
2	4	5	4	.75817	.014	.365	3.28543	.026	.062	2.55520	.023	.081
2	4	6	34	.53475	.121	.409	2.14409	.173	.098	1.71126	.159	.092
2	4	7	6	.10133	.003	.500	.49271	.006	.210	.38428	.004	.191
2	5	5	35	.88210	.047	.343	3.19041	.138	.161	2.44637	.109	.149
2	5	6	28	.20459	.023	.448	.7356	.076	.195	.55616	.058	.190
2	5	7	18	.14444	.011	.473	.52604	.027	.179	.41250	.016	.155
2	6	5	12	.96797	.010	.399	3.32241	.036	.129	2.44811	.026	.128
2	6	6	51	.32966	.036	.403	1.11817	.139	.190	.80116	.096	.168
2	7	5	15	2.09978	.049	.739	6.95018	.097	.179	4.54721	.073	.122

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

2	7	6	28	.54325	.040	.421	1.52431	.140	.198	1.02857	.090	.180
2	8	5	11	1.03444	.135	.484	2.65977	.158	.380	1.70071	.145	.127
2	8	6	40	.51158	.462	.665	1.57950	.004	.834	.96285	.523	.733
2	8	7	102	.43445	.218	.511	1.17387	.305	.565	.73381	.253	.413
3	1	2	2	.00000	.000	.000	.00001	.000	.000	.00000	.000	.333
3	1	4	5	3.44215	.582	2.000	30.23983	.578	.128	24.87926	.579	.104
3	1	5	22	.54404	.591	1.972	3.37213	.005	.194	2.82501	.603	.191
3	1	7	3	.39576	.130	1.414	1.53421	.124	.083	1.32287	.125	.000
3	2	5	79	.51694	.439	1.764	3.77433	.424	.303	3.18905	.427	.309
3	2	6	49	.07650	.461	1.982	.59068	.463	.275	.49795	.461	.271
3	2	7	41	.06087	.342	1.424	.38206	.302	.351	.32457	.309	.331
3	3	1	54	.00000	.000	.386	.00000	.031	.424	.00000	.000	.325
3	3	5	84	.51476	.244	1.023	2.21281	.212	.266	1.67653	.223	.266
3	3	7	14	.07732	.394	1.180	.34766	.329	.325	.29411	.342	.322
3	4	5	58	.36665	.214	.919	1.33294	.144	.234	1.09888	.161	.231
3	4	6	11	.45536	.031	.342	1.18788	.017	.211	.99175	.021	.197
3	4	7	52	.10608	.061	.475	.37997	.046	.236	.31231	.036	.223
3	5	6	56	.27584	.138	.546	1.01012	.049	.207	.78580	.074	.204
3	5	7	18	.23609	.009	.516	.65961	.023	.207	.52585	.013	.173
3	6	6	52	.27300	.037	.597	.91090	.081	.251	.66471	.037	.226
3	6	7	17	.21593	.021	.511	.80097	.112	.261	.57516	.077	.243
3	7	6	24	.22275	.341	.993	.96704	.461	.529	.61602	.404	.524
3	7	7	86	.29060	.063	.524	1.08161	.159	.270	.69589	.111	.231
3	8	5	8	.54430	.028	.422	2.79351	.033	.189	1.49324	.030	.261
3	8	6	33	.35575	.134	.748	1.67747	.209	.354	.94570	.149	.274
3	8	7	85	.33628	.118	.545	1.26453	.163	.354	.74957	.134	.299
4	7	6	2	.00000	.001	.000	.68786	.005	.000	.38232	.003	.000

BIN RATIOS M=4

I	J	K	NO	R	FSOI	PFSOI	R	FSOI	PFSOI	R	FSOI	PFSOI
-	1	1	3 7	2.73504	.112	.866	7.30573	.111	1.296	9.81941	.110	.980
1	1	4 87		.95987	.581	.766	3.34420	.914	1.021	3.05586	.970	.880
1	1	5 124		.51713	.305	.855	2.17472	.453	.696	1.99674	.543	.592
1	1	6 40		.33390	.508	.956	1.16806	.463	.770	1.18979	.602	.627
1	1	7 51		.21834	.170	.720	1.16710	.167	.178	.95852	.168	.177
1	2	1 1		.00000	.000	.000	.60100	.000	.000	.00000	.000	.300
1	2	4 98		.96340	.244	.671	4.71547	.237	.220	3.87334	.238	.215
1	2	6 37		.28434	.161	.513	.33444	.163	.494	.86895	.164	.323
1	2	7 134		.22629	.150	.492	.97076	.404	.548	.85311	.469	.500
1	3	1 32		.00000	.000	.341	.00000	.000	.530	.00000	.000	.275
1	3	2 77		.00000	.000	.708	.00000	.000	.353	.00000	.000	.194
1	3	3 44		.46753	.018	.745	3.47920	.021	.261	2.86647	.017	.252
1	3	4 26		1.45745	.105	.865	8.33185	.112	.220	6.79855	.110	.210
1	3	6 44		.34130	.022	.369	1.46078	.054	.109	1.20574	.050	.105
1	3	7 97		.25662	.181	.370	.87210	.570	1.135	.95223	.804	.955
1	4	1 30		.00000	.000	.353	.00000	.000	.397	.00000	.000	.305
1	4	2 18		.00000	.000	.284	.00000	.000	.334	.00000	.000	.237
1	4	3 01		29.91953	1.329	.494	5.64105	1.368	.610	11.93126	1.358	.348
1	4	4 53		1.43842	.221	.796	4.98146	.152	.297	3.98924	.171	.264
1	4	6 16		.34235	.174	.377	1.54838	.235	.359	1.28133	.302	.350
1	4	7 46		.27615	.011	.398	.38530	.629	.301	.99560	.051	.208
1	5	1 28		.00000	.000	.385	.00000	.000	.484	.00000	.000	.359
A	1	5 4 49		.76355	.162	1.057	3.63876	.077	.264	2.27446	.105	.273
A	1	5 6 14		.41012	.070	.333	.57654	.104	.419	1.42186	.134	.178
I	1	6 1 29		.00000	.000	.149	.00000	.000	.541	.00000	.000	.150
II	1	6 4 44		.91209	.108	.593	2.84726	.177	.291	2.05550	.143	.269
I	6	6 12		.74658	.140	.356	1.09979	.195	.357	2.23215	.249	.287
I	7	1 4		.00107	.000	.214	.00000	.000	.512	.00000	.000	.186
I	7	4 41		1.11826	.021	.595	3.32640	.083	.263	2.22137	.034	.227
I	7	5 6		1.57456	.033	.266	2.03925	.044	.204	6.72648	.054	.266
I	7	4 10		1.23340	.063	.369	1.64640	.087	.330	3.86591	.109	.302
I	8	4 20		1.13373	.263	.577	3.52486	.307	.379	2.19184	.242	.294
I	8	5 89		1.27193	.274	.406	3.15577	.206	.420	2.10416	.234	.282
I	8	6 14		2.17033	.286	.386	2.79593	.344	.544	2.37376	.315	.131
I	8	7 149		.78328	.409	.400	1.62634	.543	.668	1.11174	.440	.470
2	1	2 6		.00000	.000	.000	.00000	.000	1.077	.00000	.000	.769
2	1	3 25		11.36049	.948	1.317	12.57960	.945	1.247	32.30913	.942	1.025
2	1	5 27		.66759	.369	1.000	2.40104	.354	.369	2.05704	.357	.310
2	1	6 46		.30758	.152	1.402	1.27160	.136	.399	1.07957	.198	.395
2	1	7 7		.63584	.124	.745	1.09283	.119	.236	1.00609	.120	.158
2	2	1 7		.10000	.000	.222	.10000	.000	.544	.00000	.000	.149
2	3	1 25		.00000	.000	.273	.00000	.001	.684	.00000	.000	.286
2	3	2 57		.00000	.000	.243	.00000	.000	.365	.00000	.000	.206
2	4	1 18		.00000	.000	.265	.00000	.000	.439	.00000	.000	.139
2	9	1 13		24.92115	1.120	.410	5.59429	1.370	.298	10.70083	1.170	.245
2	4	5 4		.64801	.011	.365	2.60821	.021	.062	2.16206	.018	.081
2	4	6 34		.48345	.081	.409	1.94245	.133	.098	1.54946	.119	.092
2	4	7 6		.11640	.004	.500	.53686	.006	.210	.41867	.003	.191
2	5	5 35		.72418	.034	.343	2.62295	.127	.161	2.01059	.098	.149
2	5	6 28		.21343	.016	.448	.76556	.069	.195	.58034	.051	.190
2	5	7 18		.15641	.014	.473	.56969	.025	.179	.44672	.014	.195
2	6	5 12		.178314	.010	.399	2.68603	.036	.125	1.98067	.026	.128
2	6	6 51		.33120	.024	.403	1.12398	.131	.190	.80515	.088	.168
2	7	5 15		1.48862	.044	.239	4.92844	.092	.179	3.22410	.068	.122

2	7	6	28	.56236	.049	.421	1.57653	.15n	.198	1.06429	.099	.180
2	8	5	11	.76044	.094	.484	1.95697	.122	.380	1.25073	.109	.127
2	8	4	40	.53534	.454	.665	1.65488	.602	.834	1.00811	.516	.733
2	8	2102		.44092	.214	.510	1.29962	.307	.5CS	.81220	.244	.413
3	1	2	2	.00000	.0010	.000	.00100	.000	.000	.00000	.000	.333
3	1	4	5	1.43847	.374	2.010	12.56101	.369	.128	10.34083	.371	.164
3	1	5	22	.40442	.464	1.972	2.91236	.480	.194	2.110383	.477	.191
3	1	7	3	.43734	.134	1.414	1.67567	.13n	.063	1.46208	.131	.000
3	2	5	75	.25429	.305	1.764	1.78457	.297	.343	1.50697	.298	.309
3	2	6	49	.07723	.408	1.982	.57684	.421	.275	.50306	.419	.271
3	2	7	41	.06619	.345	1.424	.41553	.306	.351	.36300	.313	.331
3	3	1	54	.00000	.000	.086	.00000	.000	.424	.00000	.000	.325
3	3	5	44	.33305	.219	1.023	1.43181	.164	.266	1.21137	.175	.266
3	3	7114		.08551	.349	1.160	.38430	.322	.325	.32514	.335	.322
3	4	5	58	.29058	.16n	.919	1.65191	.086	.204	.66806	.104	.231
3	4	6	11	.34013	.022	.342	1.01758	.008	.211	.84959	.012	.197
3	4	7	52	.11724	.064	.475	.42015	.039	.236	.34529	.031	.223
3	5	6	56	.25732	.103	.546	.93921	.620	.207	.73137	.042	.204
3	5	7	18	.276289	.009	.516	.73447	.023	.207	.58553	.013	.173
3	6	6	52	.28037	.021	.597	.93392	.696	.251	.68196	.051	.226
3	8	7	17	.24040	.021	.511	.69177	.112	.261	.64034	.077	.243
3	7	6	24	.23048	.323	.993	1.60274	.443	.529	.63812	.386	.524
3	7	7	86	.31923	.057	.524	1.18763	.156	.270	.76448	.107	.231
3	8	5	8	.44506	.017	.422	2.33136	.622	.189	1.24617	.019	.261
3	8	6	33	.32914	.191	.748	1.55675	.161	.354	.87622	.122	.274
3	8	7	85	.36864	.111	.545	1.38633	.158	.354	.82173	.130	.299
4	7	6	2	.00000	.000	.000	.72202	.004	.000	.40130	.012	.000

AB-10

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

BIN RATIOS M/S			R	F501	PFS01	R	F501	PFS01	R	F501	PFS01
I	J	K NO									
1	1	3 7	1.28142	.079	.866	3.42278	.079	1.296	4.6n035	.078	.980
1	1	4 87	.60640	.522	.766	2.13922	.889	1.021	1.95843	.949	.880
1	1	5126	.42133	.240	.855	1.75402	.446	.696	1.60346	.539	.592
1	1	6 40	.32205	.504	.956	1.15914	.417	.270	1.16408	.560	.627
1	1	7 51	.23852	.157	.770	1.27480	.155	.178	1.04698	.155	.177
1	2	1 1	.000000	.000	.000	.000000	.000	.000	.000000	.000	.000
1	2	4 98	.46404	.099	.671	2.20787	.087	.220	1.86349	.089	.215
1	2	6 37	.29317	.145	.513	.34482	.146	.494	.89594	.146	.323
1	2	7 14	.25176	.156	.492	1.07416	.402	.540	.94445	.468	.500
1	3	1 32	.000000	.000	.341	.000000	.000	.530	.000000	.000	.275
1	3	2 77	41.43233	.544	.208	4.531147	.526	.353	13.47194	.531	.194
1	3	3 44	.42047	.014	.745	1.68436	.019	.263	1.38936	.011	.252
1	3	4 26	.41011	.025	.865	2.34472	.032	.220	1.91382	.030	.210
1	3	6 44	.35481	.011	.369	1.51920	.047	.109	1.25485	.039	.105
1	3	7 97	.28350	.164	.370	.45218	.587	1.135	1.03589	.818	.955
1	4	1 30	.000000	.000	.253	.000000	.000	.397	.000000	.000	.305
1	4	2 18	16.14380	.054	.284	2.23119	.050	.339	5.69416	.051	.237
1	4	3 01	.044245	.448	.494	1.30648	.463	.610	2.76580	.459	.348
1	4	4 53	.46389	.079	.796	1.59024	.009	.297	1.27711	.024	.264
1	4	6 16	.34660	.156	.377	1.55803	.234	.359	1.28791	.304	.350
1	4	7 46	.29926	.010	.398	.41762	.023	.301	1.07925	.044	.208
1	5	1 28	.000000	.000	.285	.000000	.000	.484	.000000	.000	.359
1	5	4 49	.36952	.072	1.057	1.45903	.015	.264	1.09495	.014	.273
1	5	6 14	.42281	.057	.333	.56845	.091	.419	1.46711	.124	.178
1	6	1 24	.000000	.000	.149	.000000	.000	.541	.000000	.000	.150
1	6	4 44	.49467	.036	.593	1.56114	.125	.291	1.32748	.045	.269
1	6	6 12	.73456	.121	.356	1.06887	.177	.357	2.17154	.230	.287
1	7	1 4	.000000	.000	.214	.000000	.000	.512	.000000	.000	.186
1	7	4 41	.70567	.021	.595	2.08992	.127	.263	1.39870	.077	.227
1	7	5 6	1.43057	.029	.266	1.85286	.039	.204	6.11193	.060	.266
1	7	6 18	1.14618	.057	.369	1.531120	.080	.330	3.59362	.102	.302
1	8	4 20	.18786	.245	.577	2.45245	.297	.374	1.52397	.268	.294
1	8	5 89	.99178	.240	.606	2.43218	.236	.420	1.61894	.265	.282
1	8	6 14	2.12286	.287	.386	2.73203	.346	.544	2.32108	.306	.131
1	8	7 149	.84651	.414	.400	1.77542	.554	.668	1.21489	.471	.470
2	1	2 6	.000000	.152	.000	23.21738	.151	.1077	38.55951	.150	.769
2	1	3 25	3.66204	.632	1.317	4.04968	.627	1.247	10.38790	.624	1.025
2	1	5 27	.58543	.331	1.000	2.10327	.316	.309	1.80292	.319	.310
2	1	6 44	.30652	.167	1.402	1.20876	.145	.399	1.07676	.149	.395
2	1	7 7	.68615	.130	.745	1.17917	.123	.236	1.08557	.124	.158
2	2	1 7	.000000	.010	.222	.000000	.000	.544	.000000	.000	.149
2	3	1 25	.000000	.000	.273	.000000	.000	.682	.000000	.000	.286
2	3	2 57	131.50277	.041	.253	13.45433	.046	.365	19.60565	.047	.206
2	4	1 18	.000000	.000	.265	.000000	.000	.439	.000000	.000	.239
2	4	3 13	3.59291	.112	.410	.80026	.113	.298	1.54518	.113	.245
2	4	5 4	.59600	.008	.365	2.58290	.018	.162	2.01697	.015	.081
2	4	6 34	.45960	.047	.409	1.84493	.109	.098	1.47436	.095	.092
2	4	7 6	.11979	.004	.500	.56247	.005	.210	.44428	.007	.191
2	5	5 35	.45223	.030	.293	2.36260	.122	.161	1.81072	.092	.149
2	5	6 28	.22314	.009	.448	.80067	.062	.195	.60689	.045	.190
2	5	7 18	.16841	.016	.473	.61349	.022	.179	.48105	.011	.155
2	2	8 2	.120041	.010	.488	.14130	.027	.142	.11110	.001	.124

2	7	6	28	.58400	.067	.421	1.63598	.158	.198	1.10484	.107	.180	
2	8	5	11	.64679	.078	.484	1.66524	.102	.380	1.06396	.088	.127	
2	8	6	40	.56125	.447	.465	1.73678	.596	.834	1.05735	.510	.733	
2	8	7	102	.53241	.221	.510	1.43755	.310	.505	.89902	.257	.413	
3	1	2	2	.60010	.285	.000	.60000	.284	.000	1.6588941	.263	.333	
3	1	4	5	.93308	.299	.000	6.13782	.289	.128	6.70109	.291	.104	
3	1	5	22	.34458	.411	1.972	2.14309	.414	.194	1.79420	.411	.191	
3	1	7	3	.44313	.143	1.414	1.87270	.138	.083	1.61470	.139	.000	
3	2	5	75	.18148	.277	1.764	1.27271	.271	.303	1.07488	.272	.109	
3	2	6	49	.07879	.377	1.982	.60927	.391	.275	.51349	.388	.271	
3	2	7	41	.07165	.349	1.424	.44990	.310	.351	.38218	.317	.331	
3	3	1	54	.00000	.000	.386	.00000	.000	.424	.00600	.000	.325	
3	3	5	84	.26661	.194	1.023	1.14464	.138	.266	.96867	.149	.266	
3	3	7	14	.09457	.380	1.180	.42470	.313	.325	.35438	.324	.322	
3	4	5	58	.25691	.132	.919	.92807	.058	.234	.76626	.074	.231	
3	4	6	11	.35961	.017	.342	.93793	.003	.213	.78311	.007	.197	
3	4	7	52	.12948	.071	.475	.46436	.031	.236	.38154	.027	.223	
3	5	6	56	.24935	.082	.546	.90824	.020	.207	.70769	.023	.204	
3	5	7	18	.29340	.008	.516	.81973	.024	.207	.65350	.011	.173	
3	6	6	82	.28920	.013	.521	.96191	.108	.251	.70279	.061	.226	
3	6	7	37	.26822	.020	.511	.99507	.111	.261	.71451	.074	.243	
3	7	6	24	.23926	.308	.093	1.04287	.428	.529	.66307	.371	.524	
3	7	7	86	.34984	.043	.524	1.30170	.153	.270	.83785	.104	.231	
3	8	5	8	.41314	.011	.422	2.11664	.016	.189	1.13137	.013	.261	
3	8	6	13	.31713	.064	.748	1.50236	.134	.354	.84480	.095	.274	
3	8	7	85	.40304	.103	.545	1.51583	.153	.354	.89644	.123	.299	
A1	4	7	6	2	.00000	.000	.000	.75899	.004	.000	.42185	.002	.000

11

BIN RATIOS M= 6

I	J	K	NO	R	FS01	PFS01	R	FS01	PFS01	R	FS01	PFS01	
1	1	3	7	•82263	.064	.866	2.19731	.064	1.296	2.95323	.063	.980	
1	1	4	87	•46624	.502	.766	1.05781	.880	1.021	1.51954	.942	.880	
1	1	5	124	•37563	.217	.465	1.55184	.454	.696	1.41763	.547	.592	
1	1	6	60	•31996	.511	.956	1.16044	.384	.770	1.16758	.534	.627	
1	1	7	51	•25953	.147	.770	1.36706	.146	.178	1.13918	.145	.177	
1	2	1	1	•00000	.000	.000	•00000	.000	.000	•00000	.000	.000	
1	2	4	98	•31273	.053	.471	1.52742	.050	.220	1.25524	.051	.215	
1	2	6	37	•30515	.132	.513	•35891	.133	.494	•93255	.133	.323	
1	2	7	34	•27613	.160	.492	1.18140	.401	.548	1.03918	.447	.500	
1	3	1	32	•00000	.000	.341	•00000	.000	.530	•00000	.000	.275	
1	3	2	77	14.73567	.202	.208	1.58368	.230	.353	4.71794	.237	.194	
1	3	3	44	•27431	.018	.745	1.10017	.019	.263	•90641	.010	.252	
1	3	4	26	•23796	.010	.485	1.356122	.017	.220	1.11056	.015	.210	
1	3	6	44	•37156	.014	.369	1.59142	.039	.109	1.31336	.031	.105	
1	3	7	97	•31138	.158	.370	1.03970	.001	1.135	1.12340	.830	.955	
1	4	1	30	•000001	.000	.353	•00000	.000	.397	•00000	.000	.305	
1	4	2	18	7.56850	.079	.284	1.64592	.033	.339	2.67166	.034	.237	
1	4	3	01	3.44277	.262	.494	•65151	.273	.610	1.37892	.270	.348	
1	4	4	53	•27683	.048	.796	•94685	.025	.297	•76089	.008	.264	
1	4	6	14	•34602	.140	.377	1.59343	.243	.359	1.31615	.306	.350	
1	4	7	46	•32353	.012	.398	•45154	.019	.301	1.16706	.039	.208	
1	5	1	28	198.72222	1.926	.385	17.19165	1.922	.484	105.65904	1.923	.359	
A	1	5	4	49	•24428	.037	1.057	•97744	.049	.264	•73426	.020	.273
A	1	5	6	14	•44006	.048	.333	•61266	.082	.419	1.52793	.115	.178
A-1	1	6	1	29	117.14857	.698	.149	10.35728	.693	.541	56.01945	.695	.150
A-1	1	6	4	44	•35993	.024	.593	1.12566	.124	.291	•81203	.082	.269
12	1	6	6	12	•73297	.109	.356	1.046728	.164	.357	2.16972	.217	.287
1	7	1	4	92.64961	.029	.214	10.15405	.019	.512	48.69034	.023	.186	
1	7	4	41	•54401	.047	.695	1.60795	.147	.283	1.07720	.097	.227	
1	7	5	6	1.36491	.026	.266	1.76786	.037	.204	5.83174	.047	.266	
1	7	6	10	1.11198	.053	.369	1.48469	.076	.330	3.48705	.098	.302	
1	8	4	21	•63661	.237	.577	1.95289	.292	.379	1.23174	.261	.294	
1	8	5	49	•86247	.238	.406	2.10140	.266	.420	1.39745	.292	.282	
1	8	6	14	2.12886	.290	.386	2.73789	.350	.544	2.32713	.310	.131	
1	8	7	49	•93280	.428	.400	1.93088	.563	.668	1.32239	.480	.470	
2	1	2	6	•00000	.121	.000	10.71875	.120	.1077	17.80131	.119	.769	
2	1	3	25	2.02384	.631	1.317	2.23688	.526	1.247	5.73494	.522	.025	
2	1	5	27	•54634	.308	1.000	1.94202	.292	.309	1.68199	.295	.310	
2	1	6	46	•31135	.181	1.402	1.28473	.157	.399	1.09439	.162	.395	
2	1	7	7	•71908	.133	.745	1.27135	.126	.236	1.16950	.128	.158	
2	2	1	7	•00000	.000	.222	•00000	.000	.544	•00000	.000	.149	
2	3	1	24	107.649010	1.334	.273	8.20170	1.336	.682	28.26658	1.336	.286	
2	3	2	57	30.95724	.384	.253	3.09172	.349	.305	9.14736	.357	.206	
2	4	1	18	•00000	.000	.265	•00000	.000	.439	•00000	.000	.239	
2	4	3	13	1.79657	.040	.410	•40423	.039	.298	•72775	.039	.245	
2	4	5	4	•57306	.017	.365	2.48150	.016	.062	1.97973	.013	.081	
2	4	6	34	•46233	.042	.409	1.82115	.094	.098	1.45190	.080	.092	
2	4	7	6	•12964	.004	.500	•63036	.004	.210	•49163	.002	.191	
2	5	5	35	•61876	.026	.343	•24211	.118	.161	1.71819	.089	.149	
2	5	6	28	•23467	.004	.448	•84226	.058	.195	•63836	.040	.190	
2	5	7	18	•28113	.019	.473	•65988	.020	.179	•51741	.009	.155	
2	6	5	12	•64058	.011	.399	2.26735	.036	.125	1.67069	.026	.128	
2	6	6	51	•34565	.024	.403	1.17393	.123	.190	•84067	.000	.168	
2	7	5	15	1.14017	.041	.239	3.727540	.089	.179	2.46961	.045	.122	

2	7	6	28	.61111	.063	.421	1.71094	.164	.198	1.15580	.113	.180	
2	8	5	11	.59243	.064	.484	1.52582	.088	.380	.97467	.074	.127	
2	8	6	40	.59146	.041	.465	1.83174	.592	.834	1.11465	.505	.733	
2	8	7	02	.58581	.223	.510	1.58122	.314	.505	.98906	.240	.413	
3	1	2	2	.00000	.176	.000	.00000	.194	.000	40.16498	.193	.333	
3	1	4	5	.72855	.262	2.000	6.35634	.252	.128	5.22980	.254	.104	
3	1	5	22	.31549	.359	1.972	1.96363	.373	.194	1.64372	.370	.191	
3	1	7	3	.53037	.150	1.414	2.05631	.144	.083	1.77301	.146	.000	
3	2	5	75	.15068	.264	1.764	1.05433	.261	.303	.89219	.242	.309	
3	2	6	49	.08134	.354	1.982	.02954	.369	.275	.53053	.364	.271	
3	2	7	41	.07740	.353	1.424	.48602	.314	.351	.41284	.321	.331	
3	3	1	54	66.50251	.444	.386	7.93446	.414	.424	19.18229	.421	.325	
3	3	5	84	.23550	.177	1.023	1.01013	.121	.266	.85500	.133	.266	
3	3	7	14	.1n196	.372	1.180	.46462	.306	.325	.39490	.319	.322	
3	4	5	58	.24107	.114	.919	.86975	.042	.234	.71833	.059	.231	
3	4	6	11	.34715	.014	.342	.90539	.000	.211	.75594	.0n4	.197	
3	4	7	52	.14219	.077	.475	.51022	.026	.236	.41918	.024	.223	
3	5	6	56	.24848	.068	.546	.90388	.030	.207	.70458	.015	.204	
3	5	7	18	.32502	.014	.516	.94819	.024	.207	.72403	.014	.173	
3	6	6	52	.30111	.010	.597	1.00048	.117	.251	.73127	.072	.226	
3	6	7	37	.29709	.020	.511	1.10224	.111	.261	.79144	.076	.243	
3	7	6	24	.25030	.297	.993	1.09245	.416	.529	.69415	.359	.524	
3	7	7	86	.34168	.053	.524	1.42033	.152	.270	.91416	.103	.231	
3	8	5	8	.39199	.007	.422	2.01858	.012	.189	1.07895	.009	.261	
3	8	6	33	.31484	.046	.748	1.49319	.115	.354	.83912	.077	.274	
3	8	7	85	.43887	.098	.545	1.65073	.149	.354	.97836	.118	.299	
A1	4	7	6	2	.00000	.000	.000	.80148	.004	.000	.44547	.002	.000

BIN RATIOS M=7

I	J	K	NO.	R	FS01	PFSD1	R	FS01	PFSD1	R	FS01	PFSD1
1	1	3	7	.51672	.050	.866	1.38019	.050	1.296	1.85499	.049	.980
1	1	4	87	.35892	.477	.766	1.28834	.473	1.021	1.18261	.937	.880
1	1	5	126	.34126	.194	.455	1.40130	.471	.696	1.27617	.542	.592
1	1	6	40	.33160	.516	.956	1.20974	.357	.770	1.21989	.505	.627
1	1	7	51	.30053	.134	.770	* 1.60613	.131	.178	1.31911	.132	.177
1	2	1	1	4.91659	.000	.000	.69989	.000	.000	1.63431	.000	.000
1	2	4	98	.21091	.043	.471	1.02952	.069	.220	.84617	.047	.215
1	2	6	37	.33384	.114	.513	.39266	.116	.494	1.02025	.117	.323
1	2	7	134	.32310	.167	.492	1.38746	.400	.548	1.22112	.467	.500
1	3	1	32	7.61944	.086	.241	.67984	.051	.530	2.29150	.057	.276
1	3	2	77	5.62055	.170	.208	.60228	.136	.353	1.79550	.144	.194
1	3	3	44	.17494	.019	.745	.70165	.018	.263	.57807	.010	.252
1	3	4	26	.14323	.002	.865	.81939	.007	.220	.66849	.005	.210
1	3	6	44	.40963	.009	.369	1.75511	.030	.109	1.44833	.021	.105
1	3	7	97	.36504	.144	.370	1.19875	.619	1.135	1.29526	.845	.955
1	4	1	30	8.08229	.122	.353	.64703	.063	.397	2.70972	.077	.305
1	4	2	18	.340571	.024	.284	.47061	.018	.339	1.20213	.020	.237
1	4	3	11	1.70674	.128	.494	.32098	.136	.610	.67942	.134	.348
1	4	4	53	.16976	.028	.796	.57974	.046	.297	.46608	.027	.264
1	4	6	46	.38305	.121	.377	1.70952	.247	.359	1.40744	.308	.350
1	4	7	46	.37154	.017	.398	.51063	.013	.301	1.34066	.033	.208
1	5	1	28	16.16688	.191	.385	.98754	.246	.484	5.96380	.225	.359
1	5	4	49	.16647	.009	1.057	.65376	.078	.264	.49151	.049	.273
1	5	6	14	.48153	.037	.333	.67066	.071	.419	1.67319	.103	.178
1	6	1	29	17.88985	.077	.149	1.49795	.048	.541	8.28958	.039	.150
1	6	4	44	.26034	.033	.593	.81320	.134	.291	.58692	.092	.269
1	6	6	12	.74109	.094	.356	1.10911	.149	.357	2.25647	.203	.287
1	7	1	4	19.28662	.004	.214	2.11324	.005	.512	10.13447	.000	.186
1	7	2	41	.42112	.045	.595	1.24294	.166	.283	.83311	.114	.227
1	7	5	6	1.34111	.023	.266	1.73710	.033	.204	5.73045	.044	.266
1	7	6	10	1.11872	.048	.369	1.44384	.072	.330	3.50890	.094	.302
1	8	4	20	.51579	.228	.577	1.60758	.287	.379	.99825	.254	.294
1	8	5	89	.74276	.248	.406	1.84559	.303	.420	1.22611	.327	.282
1	8	6	14	2.22395	.297	.386	2.85784	.357	.544	2.43043	.317	.131
1	8	7	149	1.08141	.440	.400	2.23450	.575	.668	1.53199	.492	.470
2	1	2	6	.00000	.095	.000	4.76145	.094	1.077	7.90749	.093	.769
2	1	3	25	1.10370	.437	1.317	1.21926	.432	1.247	3.12440	.428	1.025
2	1	5	27	.52144	.281	1.000	1.87881	.265	.309	1.61081	.268	.310
2	1	6	46	.33041	.202	1.402	1.36990	.176	.399	1.16221	.181	.395
2	1	7	7	.84496	.137	.745	1.45237	.131	.236	1.33707	.132	.158
2	2	1	7	15.90123	.038	.222	.65324	.039	.544	3.75743	.039	.149
2	3	1	25	17.40566	.381	.273	1.38177	.423	.682	4.72094	.414	.286
2	3	2	57	9.76386	.256	.253	.97015	.219	.365	2.87354	.227	.206
2	4	1	18	25.93239	.149	.265	1.02191	.072	.439	7.79289	.090	.239
2	4	3	13	.93353	.047	.410	.21007	.044	.298	.40157	.045	.245
2	4	5	4	.56806	.005	.365	2.46188	.014	.062	1.91292	.011	.081
2	4	6	34	.46236	.025	.409	1.86123	.077	.098	1.48508	.062	.092
2	4	7	6	.14907	.006	.500	.72486	.003	.210	.56533	.001	.191
2	5	5	35	.60410	.023	.343	2.18977	.114	.161	1.67789	.085	.149
2	5	6	28	.26007	.003	.448	.93372	.052	.195	.70760	.034	.190
2	5	7	18	.20665	.022	.473	.75291	.017	.179	.59034	.004	.155
2	6	5	12	.64154	.011	.399	2.20198	.036	.125	1.62253	.027	.128
2	6	6	51	.37280	.029	.403	1.26454	.120	.190	.90489	.079	.168
2	7	5	15	1.06622	.040	.239	3.53073	.087	.179	2.30950	.064	.122

2	7	6	28	.67309	.070	.421	1.88317	.171	.198	1.27258	.120	.180
2	8	5	11	.55567	.048	.484	1.43180	.070	.380	.91437	.056	.127
2	8	4	40	.65715	.435	.465	2.03720	.586	.834	1.23896	.499	.733
2	8	7	72	.68837	.277	.510	1.65724	.319	.505	1.16202	.244	.413
3	1	2	2	.nnn100	.142	.nnn	.00n0n	.141	.000	15.54654	.14n	.333
3	1	4	5	.57075	.227	2.000	4.97221	.216	.128	4.09529	.218	.104
3	1	5	22	.29526	.312	1.972	1.83924	.325	.194	1.53934	.322	.191
3	1	7	3	.62151	.158	1.414	2.40979	.153	.083	2.07777	.154	.000
3	2	5	75	.12708	.254	1.764	.89056	.254	.303	.75222	.254	.309
3	2	6	49	.08814	.374	1.982	.68218	.342	.275	.57483	.319	.271
3	2	7	41	.08874	.357	1.624	.55761	.318	.351	.47365	.324	.331
3	3	1	54	1A.70638	.324	.386	1.98361	.287	.424	4.80001	.294	.325
3	3	5	84	.21200	.154	1.023	.90827	.101	.266	.76894	.112	.266
3	3	7	14	.12202	.362	1.180	.54726	.296	.325	.46321	.319	.322
3	4	5	58	.23252	.097	.919	.83774	.024	.234	.69212	.041	.231
3	4	6	11	.34737	.011	.342	.90592	.003	.211	.75640	.001	.197
3	4	7	52	.16664	.084	.475	.59843	.019	.236	.49156	.028	.223
3	5	6	56	.25764	.052	.546	.93573	.045	.207	.72976	.020	.204
3	5	7	18	.18554	.004	.516	1.07711	.024	.207	.85870	.014	.173
3	6	6	52	.32964	.015	.697	1.09386	.128	.251	.79992	.083	.226
3	6	7	17	.36223	.019	.511	1.30490	.110	.261	.93837	.074	.243
3	7	6	24	.27559	.284	.993	1.20484	.402	.529	.76496	.346	.524
3	7	7	84	.44353	.057	.624	1.65071	.152	.270	1.06236	.104	.231
3	8	5	8	.38692	.003	.422	1.98238	.008	.189	1.05959	.005	.261
3	8	6	13	.32510	.024	.748	1.54393	.094	.354	.86699	.056	.274
3	8	7	85	.50870	.059	.545	1.91356	.144	.354	1.13407	.112	.299
4	7	6	2	.nnn000	.001	.000	.89275	.003	.000	.49620	.002	.000

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

BIN RATIOS N = 8

I	J	K	NO	R	FSD1	PFSD1	R	FSD1	PFSD1	R	FSD1	PFSD1		
1	1	3	7	.41683	.044	.866	1	11335	.043	1.296	1.49634	.043	.980	
1	1	4	87	.32240	.044	.766	1	16338	.069	1.021	1.06879	.035	.880	
1	1	5	126	.33435	.091	.855	1	36782	.482	.696	1.24455	.573	.592	
1	1	6	60	.34728	.518	.956	1	27662	.341	.770	1.28883	.492	.627	
1	1	7	51	.33607	.128	.770	1	79604	.124	.178	1.47509	.125	.177	
1	2	1	1	1.81633	.000	.000		.25556	.000	.000	.60374	.000	.000	
1	2	4	94	.17756	.061	.671		.86652	.068	.220	.71224	.067	.215	
1	2	6	37	.36174	.107	.513		.42649	.108	.494	1.05555	.108	.323	
1	2	7	134	.36384	.171	.492	1	56384	.394	.548	1.37679	.466	.500	
1	3	1	32	2.85880	.059	.341		.25488	.022	.530	.85925	.028	.275	
1	3	2	77	3.56914	.134	.208		.38416	.102	.353	1.14557	.110	.194	
1	3	3	44	.14211	.019	.745		.56997	.018	.263	.46958	.010	.252	
1	3	4	26	.11516	.004	.865		.65883	.003	.220	.53750	.002	.210	
1	3	6	44	.44576	.014	.369	1	91028	.024	.109	1.57630	.016	.105	
1	3	7	97	.41103	.136	.370	1	34017	.629	1.135	1.44500	.844	.955	
1	4	1	30	3.36707	.077	.253		.28869	.025	.397	1.12625	.031	.305	
1	4	2	18	2.32113	.018	.284		.32072	.012	.339	.61928	.013	.237	
1	4	3	101	1.22662	.077	.494		.23064	.087	.610	.48823	.084	.348	
1	4	4	53	.13743	.021	.796		.46907	.054	.297	.37716	.035	.264	
1	4	6	16	.41126	.111	.177	1	82008	.25n	.359	1.50618	.309	.350	
1	4	7	46	.41359	.020	.398		.57737	.011	.301	1.49201	.029	.208	
1	5	1	28	4.99466	.127	.385		.42797	.184	.484	2.58314	.164	.359	
1	5	4	49	.13963	.004	1.057		.54779	.089	.264	.41198	.061	.273	
1	5	6	14	.52193	.071	.133		.72707	.065	.419	1.81430	.098	.178	
1	6	1	29	8.43576	.030	.149		.70324	.077	.541	3.89878	.039	.150	
1	6	4	44	.22710	.042	.593		.70869	.143	.291	.51169	.101	.269	
1	6	6	12	.80147	.087	.356	1	16842	.142	.357	2.37807	.195	.287	
1	7	1	4	9.59090	.000	.214	1	05082	.010	.512	5.03953	.006	.186	
A1-16	1	7	4	41	.37979	.073	.695	1	11959	.174	.283	.75103	.124	.227
1	7	5	6	1.36968	.021	.266		.17744	.032	.204	.585273	.042	.266	
1	7	6	10	1.15949	.044	.369		.154836	.070	.330	3.63714	.092	.302	
1	8	4	20	.47513	.224	.577		.148131	.285	.379	.91969	.251	.294	
1	8	5	89	.73728	.258	.406	1	77773	.324	.420	1.18044	.345	.282	
1	8	6	14	2.34960	.302	.186		.301796	.362	.544	2.56737	.322	.131	
1	8	7	49	1.21007	.444	.400		.249788	.582	.668	1.71360	.499	.470	
2	1	2	6	.00000	.084	.000		.322747	.083	1.077	5.35990	.083	.769	
2	1	3	25	.83284	.393	1.417		.41981	.388	1.247	2.35648	.383	1.025	
2	1	5	27	.52761	.262	1.000		.189324	.251	.309	1.62331	.254	.310	
2	1	6	46	.35207	.215	1.402		.146042	.188	.399	1.23889	.193	.395	
2	1	7	2	.93828	.140	.745		.161280	.133	.236	1.48476	.134	.158	
2	2	1	7	.6.01574	.012	.222		.24705	.014	.544	1.42101	.013	.149	
2	3	1	25	7.63524	.164	.273		.61228	.183	.682	2.08749	.176	.286	
2	3	2	51	.6.49414	.214	.253		.56482	.176	.365	1.67359	.184	.206	
2	4	1	18	9.36510	.099	.265		.39282	.022	.439	2.80641	.038	.239	
2	4	3	13	.69736	.060	.410		.15493	.057	.298	.29998	.058	.245	
2	4	5	4	.58281	.003	.365		.2.52483	.013	.062	1.96260	.010	.081	
2	4	6	34	.48301	.017	.409	1	.94733	.048	.098	1.45192	.054	.092	
2	4	7	6	.16606	.007	.500		.80747	.003	.210	.62976	.000	.191	
2	5	5	35	.61496	.021	.343		.2.22954	.112	.161	1.70826	.083	.149	
2	5	6	28	.24380	.005	.448		.1.01908	.048	.195	.77225	.031	.190	
2	5	7	18	.22921	.023	.473		.83517	.016	.179	.65483	.004	.155	
2	6	5	12	.65133	.011	.399		.2.23559	.036	.125	1.64730	.027	.128	
2	6	6	51	.406190	.032	.413		.1.36231	.119	.190	.97536	.079	.168	
2	7	5	15	1.016264	.034	.239		.3.51896	.087	.179	2.30177	.043	.122	

2	7	6	28	.73208	.074	.421	2.04747	.175	.198	1.38387	.124	.180
2	8	5	11	.55395	.034	.484	1.42274	.060	.380	.91163	.046	.127
2	8	6	40	.71809	.431	.465	2.22731	.583	.834	1.35416	.495	.733
2	8	7102		.77612	.230	.510	2.09347	.323	.505	1.31002	.268	.413
3	1	2	2	.000100	.121	.000	.000100	.122	.000	.9.99874	.121	.333
3	1	4	5	.51753	.211	2.000	4.50744	.199	.128	3.71267	.202	.104
3	1	5	22	.29373	.246	1.972	1.83058	.300	.194	1.53196	.297	.191
3	1	7	3	.49945	.163	1.414	2.71286	.15d	.083	2.33407	.159	.000
3	2	5	25	.12003	.254	1.764	.84104	.251	.303	.71041	.251	.309
3	2	6	49	.09495	.311	1.982	.73515	.327	.275	.61944	.324	.271
3	2	7	41	.09877	.360	1.624	.6203H	.321	.351	.52697	.328	.331
3	3	1	54	A.75847	.245	.386	1.03833	.247	.424	2.51334	.254	.325
3	3	5	84	.20484	.144	1.023	.88559	.089	.266	.74986	.100	.266
3	3	7114		.13749	.357	1.180	.81634	.291	.325	.52173	.303	.322
3	4	5	58	.23526	.088	.919	.84703	.014	.234	.69991	.032	.231
3	4	6	11	.35908	.004	.342	.93643	.004	.211	.78188	.001	.197
3	4	7	52	.18760	.049	.475	.67401	.318	.236	.55358	.031	.223
3	5	6	56	.27111	.042	.546	.98387	.053	.207	.76749	.027	.204
3	5	7	18	.43698	.008	.516	1.22081	.024	.207	.97326	.014	.173
3	6	6	52	.35738	.020	.597	1.18512	.134	.251	.86688	.089	.226
3	6	7	37	.39914	.018	.511	1.48104	.109	.261	1.06338	.074	.243
3	7	6	24	.29969	.277	.993	1.31137	.395	.529	.83225	.338	.524
3	7	7	86	.49695	.060	.524	1.84968	.153	.270	1.19036	.106	.231
3	8	5	8	.39505	.001	.422	2.024JH	.006	.189	1.08187	.001	.261
3	8	6	33	.34145	.015	.748	1.62262	.082	.354	.91082	.045	.274
3	8	7	85	.56916	.085	.545	2.14114	.141	.354	1.2689P	.108	.299
4	7	6	2	.00000	.001	.000	.97687	.003	.000	.54295	.001	.000

BIN RATIOS Ma 9										
I	J	K	N	R	FSOI	PFSOI	R	FSOI	PFSOI	
1	1	3	7	•37311	.741	.866	•99654	.040	1.296	
1	1	4	87	•30746	.464	.766	1.11303	.867	1.021	
1	1	5	26	•33547	.192	.855	1.36944	.490	.696	
1	1	6	40	•16316	.571	.956	1.33819	.333	.770	
1	1	7	51	•36458	.122	.771	1.9483H	.120	.178	
1	2	1	1	1.06614	.000	.000	1.5177	.000	.000	
1	2	4	98	•16321	.093	.471	•79640	.100	.220	
1	2	6	37	•38518	.102	.513	•45305	.102	.494	
1	2	7	14	•39560	.174	.492	1.76447	.399	.548	
1	3	1	32	•69054	.094	.341	•15166	.013	.530	
1	3	2	77	2.81858	.120	.208	•30151	.045	.353	
1	3	3	44	•12769	.019	.746	•51216	.018	.263	
1	3	4	26	•10337	.005	.865	•59137	.002	.220	
1	3	6	44	•47682	.017	.369	2.03935	.021	.109	
1	3	7	97	•44772	.131	.370	1.45303	.035	1.135	
1	4	1	30	2.10013	.055	.353	•16731	.029	.397	
1	4	2	18	•88497	.015	.284	•20045	.009	.339	
1	4	3	101	•02896	.052	.494	•19346	.065	.610	
1	4	4	53	•12378	.018	.796	•42234	.058	.297	
1	4	6	16	•43550	.105	.377	1.93n64	.251	.359	
1	4	7	46	•44747	.022	.398	•62469	.010	.301	
1	5	1	24	4.43816	.096	.385	•27177	.159	.484	
1	5	4	49	•12806	.010	1.057	•50209	.096	.264	
1	5	6	14	•55804	.078	.333	•77443	.062	.419	
1	6	1	29	4.60119	.012	.149	•46569	.098	.541	
1	6	4	44	•21308	.048	.593	•66451	.150	.291	
A1	1	6	6	12	•83908	.083	.356	1.22354	.138	.357
A1	1	7	1	4	6.54495	.003	.214	•72146	.013	.512
A1	1	7	4	41	•16316	.078	.595	1.67311	.179	.283
88	1	7	5	6	1.40800	.020	.266	1.82378	.031	.204
1	7	6	10	1.20308	.045	.369	1.60663	.068	.330	
1	8	4	20	•45964	.222	.577	1.43324	.284	.379	
1	8	5	89	•73405	.265	.610	1.70645	.335	.420	
1	8	6	14	2.44660	.306	.386	3.10485	.365	.544	
1	8	7	149	1.31321	.450	.400	2.70921	.586	.668	
2	1	2	4	.00000	.078	.000	2.61346	.078	1.077	
2	1	3	25	•71811	.367	1.317	•79298	.362	1.247	
2	1	5	27	•53826	.259	1.000	1.93124	.243	.309	
2	1	6	46	•37116	.223	1.402	1.54006	.196	.399	
2	1	7	7	1.011369	.141	.745	1.74244	.134	.236	
2	2	1	7	•565577	.001	.222	1.46444	.003	.544	
2	3	1	25	4.80558	.082	.273	•38728	.073	.682	
2	3	2	57	4.24856	.193	.253	•42109	.155	.365	
2	4	1	18	5.44533	.080	.265	•22803	.014	.439	
2	4	3	13	•59983	.067	.410	•13499	.064	.298	
2	4	5	4	•60067	.003	.365	2.60328	.012	.062	
2	4	6	34	•50339	.012	.409	2.03103	.063	.098	
2	4	7	6	•17974	.007	.500	•87398	.003	.210	
2	5	5	35	•03099	.020	.343	2.28789	.111	.161	
2	5	6	28	•30343	.007	.448	1.08968	.047	.195	
2	5	7	18	•24747	.024	.473	•90174	.015	.179	
2	6	5	12	•66730	.011	.399	2.29n4n	.036	.125	
2	6	6	51	•42498	.034	.403	1.44430	.119	.190	
2	7	5	15	1.07751	.039	.239	3.56826	.087	.179	
							2.33400	.063	.122	

2	7	6	28	.78723	.074	.421	2.18447	.174	.198	1.47663	.126	.183
2	8	5	11	.56153	.030	.484	1.44752	.053	.380	.92418	.039	.127
2	8	6	40	.74838	.429	.465	2.38402	.582	.834	1.44918	.493	.733
2	8	7	102	.84607	.232	.510	2.28181	.325	.505	1.42800	.270	.413
3	1	2	2	.00000	.114	.000	.00000	.113	.000	.88467	.112	.333
3	1	4	5	.49633	.203	.20000	4.32217	.191	.128	3.56117	.193	.104
3	1	5	22	.29731	.271	.1972	1.85337	.285	.194	1.56095	.287	.191
3	1	7	3	.74201	.164	.1414	2.95470	.160	.083	2.54758	.142	.000
3	2	5	75	.11797	.241	.1764	.82455	.250	.303	.69818	.260	.309
3	2	6	42	.10075	.302	.1982	.78016	.318	.275	.45734	.315	.271
3	2	7	41	.10682	.361	.1424	.67099	.322	.351	.56995	.329	.331
3	3	1	54	.61581	.264	.386	.72953	.229	.424	1.76611	.236	.325
3	3	5	84	.20717	.137	.1023	.88419	.082	.266	.75043	.093	.266
3	3	7	14	.14982	.353	.1181	.62145	.288	.325	.56840	.300	.322
3	4	5	58	.24056	.072	.919	.06518	.013	.234	.71546	.028	.231
3	4	6	11	.37273	.018	.342	.97021	.005	.211	.81008	.002	.197
3	4	7	42	.20433	.092	.475	.73431	.018	.236	.60304	.031	.223
3	5	6	56	.28372	.039	.646	.1.02416	.056	.237	.80293	.031	.204
3	5	7	18	.47786	.007	.516	1.33504	.024	.207	1.06433	.014	.173
3	6	8	52	.38067	.023	.597	1.26184	.137	.251	.92315	.092	.226
3	6	7	37	.43644	.018	.511	1.61947	.109	.261	1.16276	.073	.243
3	7	6	24	.31977	.271	.993	1.39999	.390	.529	.88827	.334	.524
3	7	7	84	.53972	.061	.524	2.00900	.153	.270	1.29287	.107	.231
3	8	5	8	.40634	.010	.422	2.08039	.005	.189	1.11196	.002	.261
3	8	6	33	.35693	.004	.748	1.69697	.075	.354	.95233	.039	.274
3	8	7	85	.61764	.082	.545	2.32358	.140	.354	1.37699	.107	.299
4	7	6	2	.000000	.001	.000	1.04611	.003	.000	.58143	.001	.000

6-14
6-10

16-27				27-400				18-400			
BIN	RATIOS	M=10		R	FSDI	PFSDI		R	FSDI	PFSDI	
I	J	K	NO	R	FSDI	PFSDI		R	FSDI	PFSDI	
				1.35045	.039	.866		1.93607	.038	1.296	
				1.30061	.452	.766		1.09049	.866	1.021	
				1.33865	.194	.855		1.38062	.495	.696	
				1.37619	.521	.956		1.38684	.327	.770	
				1.38668	.119	.770		2.00651	.117	.178	
				1.27682	.000	.000		1.11058	.000	.000	
				1.14598	.100	.471		1.76103	.108	.220	
				1.40373	.099	.513		1.47488	.099	.494	
				1.42050	.174	.492		1.81318	.398	.548	
				1.42367	.042	.341		1.11020	.012	.530	
A1-20				1.49953	.018	.369		2.14115	.019	.104	
				1.3797	.124	.271		1.54162	.639	1.135	
				1.56343	.043	.753		1.12602	.039	.397	
				1.66556	.013	.284		1.23013	.007	.339	
				1.42845	.040	.494		1.17455	.055	.610	
				1.41687	.017	.796		1.39871	.060	.297	
				1.45490	.102	.377		2.01462	.252	.359	
				1.47379	.023	.198		1.66147	.009	.301	
				1.33774	.077	.285		1.20493	.144	.484	
				1.5449	.12219	.014	1.0057	1.47495	.099	.264	
				1.5614	.58274	.025	.333	1.81194	.060	.419	
				1.6129	1.37775	.015	.149	1.36369	.111	.541	
				1.6444	.20626	.052	.593	1.64298	.154	.291	
				1.6612	.67016	.0011	.256	1.26904	.135	.357	
				1.714	5.25889	.004	.214	1.57616	.014	.512	
				1.7441	.35572	.000	.595	1.04790	.181	.263	
				1.756	1.44325	.020	.266	1.86946	.030	.204	
				1.7610	1.24180	.044	.369	1.665703	.068	.330	
				1.8420	.45339	.221	.577	1.41392	.283	.379	
				1.8614	.73750	.270	.406	1.77257	.343	.420	
				1.8614	2.55897	.308	.286	3.28644	.367	.544	
				1.87149	1.39316	.452	.400	2.67310	.588	.668	
				2.12	.00000	.076	.000	2.30531	.074	1.077	
				2.1325	.65908	.352	1.117	1.72773	.347	1.247	
				2.1527	.54913	.254	1.000	1.97005	.238	.309	
				2.1646	.38660	.224	1.402	1.60441	.200	.399	
				2.177	1.07237	.142	.745	1.84332	.135	.236	
				2.217	2.61127	.004	.222	1.10724	.003	.544	
				2.3125	3.62751	.095	.273	1.29314	.042	.682	
				2.3257	3.56563	.182	.253	1.35324	.144	.365	
				2.4118	3.94798	.071	.265	1.16520	.020	.439	

2	4	3	13	+54630	.071	.410	+12384	.048	.298	+23673	.0	.245
2	4	5	4	+61671	.002	.365	+67281	.012	.062	+67479	.009	.081
2	4	6	34	+52058	.010	.409	+67467	.060	.098	+67314	.044	.092
2	4	7	6	+19036	.007	.500	+52564	.003	.210	+7193	.000	.191
2	5	5	35	+64604	.019	.343	+34263	.111	.161	+79482	.081	.149
2	5	6	28	+31887	.004	.448	+14522	.045	.195	+86779	.027	.190
2	5	7	16	+26164	.074	.073	+95356	.014	.179	+74764	.003	.155
2	6	5	12	+6H259	.011	.399	+34287	.034	.125	+72634	.027	.128
2	6	6	51	+44423	.017	.403	+50980	.119	.190	+08088	.079	.168
2	7	5	15	+09526	.039	.239	+62709	.086	.179	+37247	.063	.122

2	7	6	78	+82002	.077	.421	+229263	.179	.198	+54985	.128	.180
2	8	5	11	+57558	.024	.484	+4101	.049	.380	+93912	.035	.127
2	8	6	40	+60790	.424	.465	+50712	.581	.834	+52383	.492	.733
2	8	7	12	+90015	.234	.510	+42741	.326	.505	+51921	.271	.413
3	1	2	2	+00000	.109	.000	+00000	.108	.000	+84857	.107	.333
3	1	4	5	+48702	.197	2.000	+24073	.185	.128	+49314	.148	.164
3	1	5	22	+30179	.262	1.972	+88158	.275	.194	+57451	.272	.191
3	1	7	3	+81024	.168	1.414	+14175	.162	.083	+70885	.163	.006
3	2	5	75	+11759	.252	1.764	+82384	.249	.363	+69590	.249	.309
3	2	6	49	+10534	.294	1.982	+81594	.312	.275	+68752	.309	.271
3	2	7	41	+11308	.362	1.424	+71034	.323	.351	+60336	.320	.331
3	3	1	54	+49H256	.254	.186	+59063	.218	.424	+42851	.226	.325
3	1	5	84	+20876	.112	1.023	+89118	.077	.266	+75639	.088	.266
3	3	7	14	+15935	.351	1.180	+7140A	.285	.325	+60450	.298	.322
3	4	5	58	+24578	.080	.919	+88434	.011	.234	+73085	.025	.231
3	4	6	11	+3H335	.004	.342	+9972	.004	.211	+83473	.002	.197
3	4	7	52	+21726	.094	.475	+76093	.019	.236	+64132	.035	.223
3	5	6	56	+29416	.034	.546	+66A/1	.061	.207	+83230	.034	.204
3	5	7	18	+50943	.087	.516	+42341	.024	.267	+13463	.014	.173
3	6	6	52	+39911	.025	.597	+32266	.139	.251	+6773	.094	.226
3	6	7	37	+46523	.018	.511	+72634	.109	.261	+23948	.071	.243
3	7	6	24	+33563	.270	.993	+46967	.388	.529	+9347	.331	.524
3	7	7	86	+57287	.065	.524	+13244	.154	.270	+37228	.158	.231
3	8	5	8	+41617	.001	.422	+13229	.004	.189	+13970	.001	.201
3	8	6	73	+36982	.006	.748	+75872	.071	.354	+98684	.036	.274
3	8	7	85	+65522	.081	.545	+46602	.139	.354	+46079	.104	.299
4	7	6	2	+00000	.001	.000	+10047	.003	.000	+61164	.001	.000

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

Table A2 Ratio of Measured to Model Counts as a
Function of B' and L'

BIN RATIOS SUMMED OVER ANGLE, M = 1															
I	J	NO.	R(MOD)	R(EXP)	SUE	SUM	R(MOD)	R(EXP)	SUE	SDH	R(MOD)	R(EXP)	SUE	SDH	
1	1	3	.34510	.19482	.921	.493	1.14087	.96952	.231	.208	.99995	.79953	.236	.194	
1	2	2	.19823	.14344	.133	.355	.39376	.55438	.207	.347	.68942	.69465	.218	.277	
1	3	2	.22103	.25613	.042	.261	1.09790	1.07997	.091	.141	.93623	.94524	.084	.134	
1	4	2	.25024	.20744	.015	.274	.45186	.30165	.024	.231	.86643	.77092	.051	.184	
1	5	1	.33400	.33400	.087	.333	.46437	.46437	.121	.419	1.15474	1.15664	.153	.178	
1	6	1	1.06844	1.06844	.122	.356	1.63793	1.53793	.377	.357	3.09745	3.09745	.428	.287	
1	7	2	5.16896	4.25348	.152	.219	7.12359	5.73646	.166	.178	16.32830	14.43745	.178	.200	
1	8	3	1.29224	.97612	.364	.257	3.27024	1.96281	.427	.303	2.61630	1.34298	.388	.138	
2	1	3	.58897	.43585	.156	.567	1.37671	.94435	.152	.174	1.10846	.85773	.152	.143	
2	4	3	.25404	.08713	.018	.241	1.08704	.41775	.007	.156	1.28191	.31721	.013	.061	
2	5	3	.22854	.13524	.018	.239	.77275	.45714	.024	.102	.58978	.34484	.014	.094	
2	6	1	.28911	.28911	.122	.403	.98089	.98089	.184	.190	.70273	.70273	.153	.168	
2	7	1	.45363	.45363	.037	.421	1.27298	1.27298	.139	.198	.85894	.85894	.089	.180	
2	8	2	.38858	.18164	.209	.408	1.08655	1.07390	.289	.445	.67157	.66512	.241	.374	
3	1	2	.54526	.14644	.177	.165	1.79148	1.34090	.170	.082	1.09302	1.15668	.172	.000	
3	2	3	.08530	.05717	.170	.1027	.61090	.37279	.345	.177	.50535	.31717	.350	.174	
3	3	1	.06478	.06478	.178	.100	.29083	.29083	.314	.325	.24611	.24611	.326	.322	
3	4	3	.27921	.13734	.078	.315	.80659	.42778	.053	.131	.70644	.34083	.056	.125	
3	5	2	.25429	.20430	.008	.375	.80221	.54994	.033	.146	.61324	.46627	.021	.132	
3	6	2	.20258	.19473	.015	.390	.72257	.72701	.064	.181	.52376	.53255	.033	.166	
3	7	2	.21654	.22822	.069	.405	.85540	.86217	.164	.253	.55034	.55587	.119	.226	
3	8	1	.47832	.36541	.120	.362	2.51787	1.53417	.156	.158	1.22900	.86162	.135	.160	
4	1	2	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000	
4	2	2	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000	
4	3	2	.00000	.00000	.000	.000	.00000	.00010	.000	.000	.00000	.00000	.000	.000	
A2-2	4	4	1	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	5	1	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000	
4	6	2	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000	
4	7	3	1.00000	1.00000	.000	1.732	.57345	.57345	.008	1.732	.31873	.31873	.005	1.732	

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

BIN RATIOS SUMMED OVER ANGLE, MM 2

I	J	NO	R(MOD)	R(EXP)	SUE	SUM	R(MOD)	R(EXP)	SUE	SUM	R(MOD)	R(EXP)	SUE	SUM
1	1	4	46323	.24197	.225	.415	1.34362	1.18673	.233	.215	1.18176	.98581	.242	.199
1	2	2	.21873	.21346	.124	.355	.43728	.39302	.194	.347	.76212	.77112	.206	.277
1	2	2	.25110	.28459	.050	.201	1.23414	1.20067	.099	.141	1.05340	1.01603	.093	.134
1	4	2	.27406	.23114	.015	.274	.49944	.34911	.037	.231	.95180	.86746	.062	.184
1	5	1	.37817	.37877	.096	.333	.52645	.52445	.129	.419	1.31089	1.31089	.161	.178
1	A	1	.91121	.91121	.225	.356	1.31846	1.31846	.201	.357	2.66425	2.66425	.333	.287
1	7	2	2.78428	2.711459	.055	.219	3.04307	3.05142	.064	.178	7.9349	8.52774	.076	.200
1	8	4	1.62017	1.39899	.277	.236	4.62342	2.83607	.313	.219	3.06446	1.99382	.284	.120
2	1	3	.56378	.45679	.114	.567	1.39359	1.11509	.117	.174	1.14636	1.00328	.117	.143
2	4	1	.25323	.10352	.016	.241	1.69932	.51893	.004	.056	1.18922	.37535	.015	.061
2	5	1	.24063	.15894	.014	.239	.82130	.56021	.030	.102	.62725	.41742	.014	.094
2	A	2	.53293	1.013136	.012	.284	2.09215	3.00148	.040	.106	1.42709	2.24161	.030	.103
2	7	2	1.22330	.70491	.034	.216	2.79808	2.73144	.092	.113	2.15222	1.64483	.045	.103
2	8	3	.61220	.60341	.160	.313	1.85731	1.77255	.200	.298	1.59406	1.07513	.177	.149
3	1	2	.49506	.19104	.164	.165	1.82171	1.83494	.158	.082	1.2009	1.32364	.159	.000
3	2	1	.09359	.06381	.346	.027	.66922	.41620	.325	.177	.55303	.35406	.329	.174
3	3	2	.14549	.10483	.346	.775	.67181	.46702	.305	.207	.56545	.39950	.313	.206
3	4	3	.25128	.18926	.047	.315	.77568	.61062	.033	.111	.63518	.45506	.031	.125
3	5	2	.25419	.21879	.011	.375	.79201	.65675	.028	.146	.61090	.50159	.018	.132
3	A	2	.22176	.21264	.020	.390	.79453	.60724	.061	.181	.57561	.59487	.028	.166
3	7	2	.24163	.25338	.072	.485	.95311	.95919	.167	.253	.61300	.61800	.122	.226
3	8	3	.42072	.49524	.057	.362	2.08015	2.29362	.064	.158	1.07207	1.25403	.062	.160
4	1	2	.00000	.00000	.000	.660	.00000	.00000	.000	.000	.000	.00000	.000	.000
A2-3	4	2	.00040	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	4	.000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	5	.000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	6	2	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.001	.000
4	7	4	1.00000	1.00000	.002	.2000	.64188	.64188	.010	.2000	.35686	.35476	.016	.2000

BIN RATIOS SUMMED OVER ANGLE, M= 3

I	J	IND	R(MOD)	R(LAB)	SDE	SDM	R(MOD)	R(EXP)	SDE	SDM	R(MOD)	R(EXP)	SDE	SDM
1	1	5	.41948	.31410	.195	.374	1.47327	1.46802	.205	.222	1.31519	1.24110	.218	.202
1	2	3	.32072	.24588	.134	.317	.99784	.44181	.203	.206	1.52n19	.89824	.211	.178
1	3	3	.33363	.45494	.021	.254	1.75804	3.46142	.034	.125	1.4954	3.29907	.028	.119
1	4	3	.40704	.25847	.022	.243	.69197	.39491	.051	.223	1.40743	.96965	.080	.164
1	5	2	.41634	.42334	.113	.358	1.39776	.60404	.154	.229	2.20267	1.52920	.192	.153
1	6	2	1.17326	.93252	.202	.316	2.36423	1.43n17	.254	.226	3.94316	2.90136	.302	.197
1	7	3	1.42935	1.78375	.041	.213	2.87179	2.74n78	.044	.151	5.94193	6.26209	.056	.191
1	8	4	1.37056	1.51402	.177	.236	3.40776	3.35950	.182	.239	2.416-3	2.31791	.170	.120
2	1	3	.63371	.45184	.101	.567	1.38758	1.22n91	.094	.174	1.16858	1.08672	.197	.143
2	4	3	.25734	1.2074	.005	.241	1.60852	.60207	.008	.050	1.14849	.43986	.065	.061
2	5	3	.25166	.18070	.011	.239	.86564	.63480	.030	.102	.66189	.47672	.019	.094
2	6	2	.44302	.47876	.011	.284	1.86640	2.37n98	.040	.106	1.29455	1.64855	.029	.103
2	7	2	1.02947	.81590	.031	.216	2.58466	2.83n95	.081	.133	1.94678	1.79172	.057	.103
2	8	3	.58513	.44497	.124	.313	1.69187	1.81n79	.154	.298	1.24756	1.11732	.136	.149
3	1	3	.59861	.48169	.156	1.010	2.59870	1.97182	.151	.069	1.32492	1.69822	.152	.060
3	2	3	.09496	.09127	.233	1.027	.67537	.60472	.221	.177	.56n05	.51452	.224	.174
3	1	2	.14187	.15774	.224	.776	.64801	.71341	.181	.207	.546n0	.60135	.191	.206
3	4	3	.23518	.22487	.032	.315	.72262	.77786	.020	.131	.593.8	.57201	.021	.125
3	5	2	.25388	.23814	.012	.375	.79839	.74157	.022	.146	.620n9	.55278	.016	.132
3	6	2	.23897	.23392	.019	.370	.85344	.86124	.067	.181	.61833	.63264	.035	.166
3	7	2	.26294	.27741	.075	.485	1.03967	1.04931	.167	.253	.66936	.67698	.123	.226
3	8	3	.39296	.46257	.034	.362	1.88250	2.2242L	.042	.158	.99456	1.21331	.037	.160
4	1	3	.00100	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	2	3	.00000	.00000	.010	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	3	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	4	2	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	5	2	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	6	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	7	4	1.00000	1.00000	.001	2.000	.68786	.68786	.009	2.000	.38232	.38232	.006	2.000

BIN RATIOS SUMMED OVER ANGLE, R= 4															
I	J	NO	R(MOD)	R(EXP)	SDE	SUM	R(MOD)	R(EXP)	SDE	SOM	R(MOD)	R(EXP)	SDE	SOM	
1	1	5	.45521	.49231	.102	.374	1.45130	2.14930	.1n9	.292	1.29447	1.99470	.114	.202	
1	2	3	.31616	.30690	.102	.317	.94351	.58929	.134	.206	1.37n25	1.17189	.139	.178	
1	3	4	.36014	.514n7	.017	.263	2.06294	2.64250	.027	.1n9	1.74263	2.32125	.019	.104	
1	4	4	.47468	.29139	.014	.237	.97582	.49216	.044	.180	1.7367	1.23765	.067	.140	
1	5	2	.46172	.47683	.069	.358	1.13693	1.07128	.062	.229	1.66947	1.80114	.084	.153	
1	6	2	.40831	.83718	.086	.315	1.66164	1.62303	.131	.226	2.13730	2.11663	.128	.197	
1	7	3	1.33874	1.25431	.018	.213	2.16024	2.12486	.037	.151	3.374.4	3.111016	.030	.151	
1	8	4	1.17543	1.22253	.149	.234	2.71177	2.77430	.154	.239	1.99470	1.90003	.151	.120	
2	1	4	.63634	.48091	.167	.524	1.48560	1.33282	.1n7	.186	1.27597	1.18644	.163	.153	
2	2	4	.35000	.14453	.000	.208	1.68343	.66451	.019	.058	1.27429	.4H064	.065	.061	
2	5	3	.25443	.20472	.011	.239	.89703	.67721	.028	.1n2	.68647	.50807	.017	.094	
2	6	2	.46646	.56108	.010	.284	1.73344	.87n90	.040	.1n6	1.21362	1.4H070	.029	.103	
2	7	2	.97201	.83722	.033	.216	2.45337	2.72460	.081	.133	1.77n05	1.76349	.057	.103	
2	8	3	.57587	.62727	.113	.313	1.61718	1.70309	.137	.298	1.09498	1.86743	.115	.149	
3	1	3	.53247	.50692	.142	1.010	2.56075	2.23447	.139	.069	1.46395	1.91809	.139	.000	
3	2	3	.09340	.09758	.201	1.027	.66117	.65421	.197	.177	.551.8	.55765	.194	.174	
3	3	2.	.14204	.16311	.198	.775	.64278	.74661	.154	.207	.54215	.62683	.162	.206	
3	4	3	.23005	.25000	.026	.315	.70449	.82714	.011	.131	.58005	.61825	.014	.125	
3	5	2	.26015	.26245	.011	.375	.82451	.83125	.015	.146	.64498	.61506	.014	.132	
3	6	2	.75732	.25194	.016	.390	.91276	.91400	.073	.181	.66146	.66464	.043	.166	
3	7	2	.28176	.30169	.069	.486	1.11808	1.13331	.163	.253	.72n95	.73298	.118	.226	
3	8	3	.38019	.42118	.022	.362	1.78718	2.06981	.03n	.158	.95726	1.12410	.025	.160	
A	4	1	3	.00000	.00000	.100	.000	.00000	.00000	.000	.000	.000.0	.01nn00	.000	.000
	4	2	4	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
B	4	3	4	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	4	2	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
C	4	5	2	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	6	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
D	4	7	4	1.00000	1.00000	.000	.2000	.72202	.72202	.008	.2000	.40130	.40130	.065	.2000

BIN RATIOS SUMMED OVER ANGLE, NO. 5														
I	J	NO.	R(MOD)	R(EXP)	SDE	SUM	R(MOD)	R(EXP)	SDE	SDM	R(MOD)	R(EXP)	SDE	SDM
1	1	5	.41138	.44567	.083	.374	1.43769	1.97096	.090	.222	1.28453	1.96979	.093	.202
1	2	1	.30511	.33234	.072	.317	.87676	.76344	.083	.206	1.2075	1.26976	.086	.178
1	3	5	.44589	.40327	.012	.176	1.80319	1.79301	.021	.1n5	1.7046	1.46185	.015	.091
1	4	5	.62017	.50368	.010	.187	.47404	.98007	.012	.159	1.62404	1.49616	.027	.121
1	5	2	.40870	.29730	.045	.354	.92810	1.20485	.018	.229	1.29120	1.12393	.018	.153
1	6	2	.62438	.53438	.039	.314	1.29436	1.31136	.104	.226	1.4695	1.29523	.088	.197
1	7	3	1.1n526	.97253	.019	.213	1.81502	1.78494	.038	.151	2.44861	2.801627	.040	.151
1	8	4	1.05919	1.02279	.142	.236	2.33963	2.36987	.163	.239	1.76541	1.62523	.155	.120
2	1	5	.66880	.57914	.090	.464	1.59465	1.81947	.085	.191	1.42137	1.66461	.086	.155
2	3	1	131.40277	131.40277	1.051	.253	13.45833	13.45833	1.046	.365	39.60565	39.60565	1.047	.206
2	4	4	.35266	.17784	.008	.204	1.43008	.71447	.007	.058	1.17617	.51559	.004	.061
2	5	1	.26887	.22559	.009	.239	.93326	.71465	.026	.102	.71444	.53492	.014	.094
2	6	2	.46476	.52053	.010	.284	1.67072	1.92952	.039	.106	1.17599	1.38042	.028	.103
2	7	2	.88467	.84278	.034	.216	2.39864	2.66301	.081	.173	1.7046	1.74261	.058	.103
2	8	3	.47870	.60604	.089	.313	1.59287	1.61484	.117	.298	1.02419	1.02093	.100	.149
3	1	4	.60702	.56723	.123	.737	2.41057	1.86832	.120	.077	1.61696	2.60902	.120	.000
3	2	1	.09311	.09754	.196	1.027	.65694	.66396	.183	.177	.54952	.56356	.184	.174
3	3	2	.14449	.16509	.182	.775	.64912	.75370	.136	.207	.54795	.63217	.145	.206
3	4	3	.23371	.26724	.021	.315	.70536	.85473	.005	.131	.58160	.65071	.009	.125
3	5	2	.27020	.28870	.011	.375	.86180	.86448	.015	.146	.6773	.67278	.012	.132
3	6	2	.27750	.28066	.011	.390	.97789	.97797	.078	.181	.70849	.70808	.049	.166
3	7	2	.30169	.32147	.064	.485	1.20113	1.22183	.159	.253	.71537	.79211	.115	.226
3	8	1	.37756	.29607	.015	.362	1.75225	1.97195	.022	.158	.94719	1.06745	.018	.160
4	1	1	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	2	5	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	3	5	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
A2	4	4	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
1	4	5	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
6	4	1	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
4	7	4	.00000	.00000	.000	.000	.75899	.75899	.008	.2000	.42105	.42185	.004	.2000

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

BIN RATIOS SUMMED OVER ANGLE, H= 7												
I	J	NO	R(IMOD)	R(EXP)	SDE	SDM	R(IMOD)	R(EXP)	SDE	SDM	R(IMOD)	
1	1	5	.35594	.40519	.061	.374	1.46083	1.40424	.066	.222	1.31A38	1.58784
1	2	3	.28508	.25493	.057	.317	.77106	.67783	.068	.206	.95845	.92272
1	3	6	.50466	.16721	.003	.157	.94669	.82785	.009	.106	1.08710	.72191
1	4	6	.2533	.19084	.015	.164	.56950	.51122	.014	.148	.96201	.87467
1	5	3	.54181	.19661	.012	.264	.72003	.69236	.054	.210	1.06910	.71746
1	6	3	1.06260	.41017	.032	.156	1.01254	1.20238	.049	.214	1.59947	1.75582
1	7	4	1.34645	2.66114	.008	.156	1.55710	1.49043	.007	.149	2.27204	9.74157
1	8	4	.94110	.40774	.142	.236	1.96810	1.98209	.177	.219	1.54249	1.34427
2	1	5	.65543	.46538	.078	.464	1.59946	1.93187	.074	.191	1.52944	2.01405
2	2	1	15.00723	15.40723	.038	.222	.65324	.65324	.039	.544	3.7573	3.76743
2	3	2	12.37601	11.48459	.217	.186	1.08266	1.07979	.204	.336	3.43629	3.33546
2	4	5	.50950	.28474	.005	.167	1.00172	.73782	.005	.061	1.08977	.59465
2	5	3	.30716	.26770	.004	.239	1.07494	.84694	.020	.102	.82309	.62761
2	6	2	.47218	.53492	.011	.284	1.70397	1.88218	.039	.106	1.20919	1.35347
2	7	2	.87988	.48011	.036	.216	2.49498	2.72110	.082	.113	1.73468	1.80115
2	8	3	.62462	.58040	.061	.313	1.66354	1.52970	.091	.298	.98810	.96896
3	1	4	.57368	.58615	.095	.737	2.50816	1.71879	.094	.077	2.07925	3.17487
3	2	3	.09854	.10161	.178	1.027	.49173	.69752	.173	.177	.58173	.59086
3	3	3	.37682	.23103	.142	.392	.83982	.89026	.103	.188	.812.2	.80595
3	4	3	.24982	.30125	.015	.315	.76088	.84925	.004	.131	.62083	.74447
3	5	2	.31059	.36212	.010	.375	1.00137	1.02309	.022	.146	.79423	.80076
3	6	2	.34144	.13433	.012	.390	1.18894	1.19907	.084	.181	.86142	.86760
3	7	2	.36641	.40271	.067	.485	1.46750	1.49467	.156	.263	.9491	.97461
3	8	3	.40253	.38194	.005	.362	1.83098	1.93764	.012	.158	1.00411	1.04328
4	1	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.0000	.00000
4	2	6	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	3	6	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	4	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	5	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	6	4	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	7	4	1.00000	1.00000	.001	2.000	.89275	.89275	.007	2.000	.49610	.49620

BIN RATIOS SUMMED OVER ANGLE, 1W 8														
I	J	NO.	R(MOD)	R(EXP)	SDE	SUM	R(MOD)	R(EXP)	SDE	SUM	R(MOD)	R(EXP)	SDE	SUM
1	1	5	+34747	+37705	+050	+374	+150091	+124247	+060	+222	+135740	+144760	+062	+202
1	2	3	-28246	-24717	-063	-317	-75142	-63319	-075	-206	-904-8	-87784	+076	+178
1	3	4	+45345	+14779	+006	+157	+68332	+58249	+005	+106	+855-2	+57316	+003	+087
1	4	5	+57823	+35690	+013	+164	+41310	+37802	+010	+148	+75n-2	+75341	+013	+112
1	5	3	+60740	+15703	+006	+264	+54848	+58998	+054	+210	+92253	+68408	+053	+144
1	6	3	+95519	+55474	+025	+158	+81887	+78467	+064	+214	+132977	+145782	+042	+125
1	7	4	+128417	+17046	+000	+156	+137861	+19418	+013	+149	+1.984-3	+4.15879	+009	+119
1	8	4	+91617	+77543	+144	+236	+142969	+144063	+181	+239	+1.52999	+1.30836	+147	+120
2	1	5	+66284	+69917	+075	+464	+142378	+185471	+071	+191	+1.60451	+2.08764	+072	+155
2	2	1	+6-n1574	+6-n1474	+012	+222	+24705	+24705	+014	+544	+1.42101	+1.42101	+013	+149
2	3	2	+648696	+648234	+126	+186	+58052	+58709	+127	+336	+1.82502	+1.84239	+127	+169
2	4	5	+52097	+33794	+004	+167	+82128	+71967	+005	+n61	+1.00156	+64367	+001	+061
2	5	3	+33263	+30n73	+006	+239	+1.16692	+92865	+019	+102	+89479	+68612	+006	+094
2	A	2	+99640	+66485	+011	+284	+1.78322	+1.94663	+039	+1n6	+1.26818	+1.40340	+028	+103
2	7	2	+91314	+91378	+034	+216	+2.62410	+2.84206	+082	+133	+1.81457	+1.88064	+059	+103
2	8	3	+66239	+58417	+051	+313	+1.74611	+1.54227	+080	+298	+1.01447	+97509	+063	+149
3	1	4	+57711	+49265	+089	+737	+2.60398	+1.70001	+087	+n77	+2.34n00	+3.24389	+087	+000
3	2	3	+10364	+10474	+175	+1.027	+72663	+72477	+170	+177	+61232	+61784	+171	+174
3	3	3	+39454	+24393	+131	+397	+79898	+84470	+092	+188	+815-8	+81176	+100	+174
3	4	3	+26580	+32138	+013	+315	+80825	+86A34	+005	+131	+66847	+77103	+001	+125
3	5	2	+33681	+40070	+009	+374	+1.08938	+1.134n3	+024	+146	+866-3	+89072	+013	+132
3	6	2	+37873	+37794	+013	+390	+1.31391	+1.33150	+084	+181	+95159	+96435	+057	+166
3	7	2	+40490	+44458	+070	+485	+1.62469	+1.65961	+156	+253	+1.05198	+1.07966	+114	+226
3	8	3	+42643	+39231	+002	+362	+1.92797	+1.99633	+009	+158	+1.06242	+1.07321	+005	+160
4	1	3	+00000	+00000	+000	+000	+00000	+00000	+000	+000	+00000	+00000	+000	+000
4	2	6	+00300	+00100	+000	+000	+00000	+00000	+000	+000	+00000	+00000	+000	+000
4	3	4	+00000	+00000	+000	+000	+00000	+00000	+000	+000	+00000	+00000	+000	+000
4	4	3	+000000	+00f00	+000	+000	+00000	+00000	+000	+000	+00000	+00000	+000	+000
4	5	3	+000000	+000000	+000	+000	+00000	+00000	+000	+000	+00000	+00000	+000	+000
4	6	4	+000000	+00100	+000	+000	+00000	+00000	+000	+000	+00000	+00000	+000	+000
4	7	4	+1.000000	+1.000000	+001	+2.000	+97687	+97687	+004	+2.000	+54295	+54295	+003	+2.000

BIN RATIOS SUMMED OVER ANGLE, N= 9												
I	J	NO.	R(MOD)	R(EXP)	SDE	SDM	R(MOD)	R(EXP)	SDE	SDM	R(MOD)	R(EXP)
1	1	5	.34593	.26197	.n53	.374	1.54049	1.15805	.056	.222	1.39479	1.37177
1	2	3	.28313	.24829	.066	.317	.74633	.62588	.078	.206	.88104	.87368
1	3	6	.42437	.14171	.nn7	.157	.54822	.46996	.003	.106	.72956	.49489
1	4	6	.54715	.34135	.n11	.166	.33436	.30918	.009	.148	.64203	.64145
1	5	3	.48940	.17267	.n12	.264	.45210	.56747	.053	.210	.84259	.64539
1	6	3	.89909	.89408	.015	.156	.70701	.63752	.072	.214	1.18393	1.13152
1	7	4	1.75306	3.16267	.004	.156	1.26612	.93173	.015	.149	1.83396	3.11500
1	8	4	.94461	.76698	.145	.236	1.93266	1.94146	.183	.239	1.542-8	1.301383
2	1	5	.67233	.72203	.n72	.464	1.64907	1.78273	.069	.191	1.66706	2.11470
2	2	1	3.56577	3.56577	.n11	.222	.14644	.14644	.003	.544	.84230	.84230
2	3	2	4.49928	4.62737	.081	.166	.40864	.39744	.070	.336	1.27671	1.29478
2	4	5	.52926	.18350	.004	.167	.71258	.62190	.004	.n61	.94528	.69265
2	5	3	.35386	.32734	.007	.239	1.24326	.99580	.018	.102	.95351	.73443
2	6	2	.51943	.48974	.n12	.264	1.45934	2.01622	.039	.1n6	1.32566	1.45600
2	7	2	.94725	.95194	.n36	.216	2.74359	2.95178	.082	.133	1.86982	1.95629
2	8	1	.49541	.49279	.043	.313	1.82200	1.56759	.074	.298	1.045-2	.98925
3	1	4	.58484	.59492	.n80	.737	2.69796	1.69543	.084	.n77	2.54864	3.26161
3	2	3	.10831	.10470	.173	1.027	.75856	.75944	.169	.177	.63973	.64275
3	3	3	.40871	.26358	.125	.392	.76252	.80416	.046	.188	.81358	.81089
3	4	3	.21977	.23640	.n12	.315	.44982	.89541	.005	.131	.70315	.79170
3	5	2	.35849	.43058	.n09	.375	1.16202	1.22654	.024	.146	.92565	.96433
3	6	2	.40882	.40496	.n14	.390	1.41516	1.43879	.084	.181	1.02489	1.04284
3	7	2	.43612	.47103	.072	.485	1.75190	1.78932	.156	.253	1.13405	1.16408
3	8	3	.44773	.40566	.000	.362	2.01705	2.06043	.0117	.158	1.11508	1.11487
4	1	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	2	6	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	3	4	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	4	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	5	3	.00000	.00100	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	6	4	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000
4	7	4	1.00000	1.00000	.002	2.000	1.04611	1.04611	.006	2.000	.58143	.58143

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

BIN RATIOS SUMMED OVER ANGLE, H= 10															
	I	J	NO.	R(1H01)	R(EXP)	SDE	SDM	R(MOD)	R(EXP)	SDE	SDM	R(MOD)	R(EXP)	SDE	SDM
	1	1	5	.34674	.15345	.051	.374	1.57414	1.11077	.054	.222	1.42691	1.32854	.055	.202
	1	2	3	.28480	.25127	.067	.317	.74661	.62841	.079	.206	.87042	.87977	.080	.178
	1	3	4	.40664	.13841	.008	.157	.47264	.45894	.002	.106	.65483	.46896	.002	.087
	1	4	4	.52901	.73680	.010	.166	.29004	.27617	.008	.148	.58215	.56577	.010	.112
	1	5	1	.47906	.18675	.014	.264	.39558	.44891	.051	.210	.79496	.45049	.052	.144
	1	6	3	.86596	.40678	.017	.155	.64019	.56245	.075	.214	1.09649	1.00626	.061	.125
	1	7	4	1.23374	2.47423	.006	.156	1.19692	.80272	.014	.149	1.74299	2.66494	.013	.119
	1	8	4	.95597	.76642	.346	.234	1.94721	1.95444	.184	.239	1.56143	1.30919	.169	.120
	2	1	5	.48100	.73787	.071	.464	1.67097	1.72808	.048	.191	1.71734	2.12458	.068	.155
A2-10	2	2	1	2.61127	2.61127	.005	.222	.10724	.10724	.003	.544	.61484	.61484	.003	.149
	2	3	2	3.49512	3.40065	.088	.186	.32966	.30478	.046	.336	1.02580	1.00979	.054	.169
	2	4	6	.53501	.41718	.063	.167	.44489	.63070	.004	.061	.90814	.73447	.001	.061
	2	5	3	.37053	.34774	.008	.239	1.30341	1.04848	.017	.102	.99977	.77236	.005	.094
	2	6	2	.53876	.61301	.012	.264	1.42297	2.07664	.039	.106	1.37173	1.50126	.028	.103
	2	7	2	.97643	.48604	.037	.214	2.84213	3.04931	.082	.133	1.95268	2.01937	.060	.103
	2	8	3	.72205	.40164	.038	.313	1.88448	1.59310	.669	.298	1.67226	1.00385	.051	.149
	3	1	4	.59264	.41660	.083	.737	2.76216	1.69551	.082	.077	2.76892	3.27019	.082	.000
	3	2	3	.11207	.11207	.171	.1027	.78452	.78393	.168	.077	.66247	.66136	.169	.174
	3	3	3	.41950	.26087	.121	.392	.73457	.77442	.082	.188	.81026	.80884	.090	.174
	3	4	1	.29104	.34939	.011	.315	.88338	.92175	.005	.131	.73113	.81191	.003	.125
	3	5	2	.37575	.45124	.009	.375	1.21916	1.29624	.025	.146	.97236	1.02371	.014	.132
	3	6	2	.43221	.43504	.015	.390	1.49405	1.52735	.084	.181	1.08200	1.10400	.058	.166
	3	7	2	.46146	.50393	.074	.465	1.85096	1.89013	.154	.253	1.19935	1.22960	.115	.226
	3	8	1	.46504	.41131	.001	.362	2.09031	2.11688	.004	.158	1.15706	1.13463	.002	.160
	4	1	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	2	6	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	3	4	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	4	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	5	3	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	6	4	.00000	.00000	.000	.000	.00000	.00000	.000	.000	.00000	.00000	.000	.000
	4	7	4	1.00000	1.00000	.002	.2000	1.10047	1.10047	.004	.000	.61164	.61164	.003	.2000

Table A3 Ratio of Measured to Model Counts in the
East and West Directions as a Function of
 B' and L'



REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

Ma 1 E,B,L RATIOS OF OBSERVED TO VETTE

I	J	NO.	18-27	27-400	18-400	NO	18-27	27-400	18-400
1	1	331 RE	.5988	2.00009	1.8118	0 RW	.0000	.0000	.0000
		FSU	2.00042	2.1368	2.1355	FSU	.0000	.0000	.0000
2	1	111 RE	.4297	1.8409	1.6074	0 RW	.0000	.0000	.0000
		FSU	1.7158	1.3418	1.3183	FSU	.0000	.0000	.0000
3	1	32 RE	2.1133	12.4962	10.7033	0 RW	.0000	.0000	.0000
		FSU	3.2141	2.5506	2.5422	FSU	.0000	.0000	.0000
4	1	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	2	270 RE	.2173	.9435	.8515	0 RW	.0000	.0000	.0000
		FSU	1.0693	1.3189	1.3528	FSU	.0000	.0000	.0000
2	7	7 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.2215	.5444	.4491	FSU	.0000	.0000	.0000
3	2	165 RE	.1085	.7549	.6390	0 RW	.0000	.0000	.0000
		FSU	2.1212	1.1831	1.1842	FSU	.0000	.0000	.0000
A3-2	4	2 0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	3	215 RE	.2364	1.0105	.9646	105 RW	.0000	.0000	.0000
		FSU	1.0359	1.3217	1.3638	FSU	.4127	.5391	.4098
2	3	15 RE	.0000	.0000	.0000	67 RW	.0000	.0000	.0000
		FSU	.2843	.4133	.2428	FSU	.2573	.3675	.2069
3	3	198 RE	.1265	.5615	.4674	54 RW	.0000	.0000	.0000
		FSU	1.4912	1.0029	1.0693	FSU	.3864	.4236	.3254
4	3	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	4	121 RE	.2592	1.0149	1.3893	143 RW	.0000	.0000	.0000
		FSU	1.3549	1.6386	1.6972	FSU	.4292	.5463	.3767
2	4	44 RE	.6470	2.6250	2.6899	31 RW	.0000	.0000	.0000
		FSU	.8292	.7084	.7099	FSU	.6206	.4031	.4974
3	4	121 RE	.1883	.6564	.5404	0 RW	.0000	.0000	.0000
		FSU	1.3171	1.1074	1.1040	FSU	.0000	.0000	.0000
4	4	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	5	63 RE	.5195	2.5757	4.6554	28 RW	.0000	.0000	.0000
		FSU	2.2371	1.9173	1.9161	FSU	.3851	.4845	.3588

2	5	81	RE	.3978 FSU	1.4099 1.0112	1.1881 .9620	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000		
3	5	74	RE	.2890 FSU	.8251	.9930 .5903	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000		
4	5	0	RE	.0000 FSU	—	.0000 .0000	0	Rw FSU	.0000 .0000	.0000 .0100	/0000 /1000		
1	6	56	RE	1.7878 FSU	2.3038	7.0996 2.1029	14.7608 2.1440	29	Rw FSU	.0000 .1490	.0000 .5407	/0000 /1495	
2	6	63	RE	.3904 FSU	.6715	1.3747 .6068	.9801 .5868	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000	
3	6	89	RE	.2074 FSU	.5774	.7253 .3135	.5254 .2836	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000	
4	6	0	RE	.0000 FSU	—	.0000 .0000	.0000 .0000	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000	
1	7	57	RE	6.4639 FSU	2.0860	19.2434 1.9199	51.1461 1.9438	4	Rw FSU	.0000 .2135	.0000 .4121	/0000 /1856	
2	7	43	RE	.7368 FSU	.8192	2.2480 .7961	1.4843 .7714	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000	
A3	3	7	110	RE	.2300 FSU	.4694	.8711 .4526	.5601 .4184	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000
4	7	2	RE	.0300 FSU	.0007	.5735 .01046	.3187 .0028	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000	
1	8	272	RE	.8637 FSU	1.1674	1.9069 1.3244	1.2584 1.1894	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000	
2	8	153	RE	.3971 FSU	.7045	1.1161 .8351	.6915 .7154	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000	
3	8	126	RE	.3040 FSU	.8434	1.1939 .6826	.7005 .4553	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000	
4	8	0	RE	.00000 FSU	.00000	.00000 .00001	.00000 .00000	0	Rw FSU	.0000 .0000	.0000 .0000	/0000 /0000	

Ms 2 E,B,L RATIOS OF OBSERVED TO VETTE

I	J	NO	18-27	27-400	18-400	NO	18-27	27-400	18-400
1	1	331 RE	.5532	2.0483	1.8002	0 RW	.0000	.0000	.0000
		FSD	1.7241	1.9012	1.9108	FSU	.0077	.0050	.0000
2	1	111 RE	.5900	1.7330	1.5114	0 RW	.0000	.0000	.0000
		FSD	1.5919	1.1752	1.1491	FSU	.0000	.0003	.0000
3	1	32 RE	.9409	5.7235	4.8804	0 RW	.0010	.0000	.0000
		FSD	2.3224	1.2419	1.2263	FSU	.0000	.0000	.0000
4	1	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSD	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	2	270 RE	.2384	1.0285	.9273	0 RW	.0000	.0000	.0000
		FSD	1.0683	1.3710	1.3541	FSU	.0000	.0000	.0000
2	2	7 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSD	.2215	.5444	.1491	FSU	.0000	.0000	.0000
3	2	165 RE	.1187	.8266	.6995	0 RW	.0000	.0000	.0000
		FSD	2.1073	1.1489	1.1497	FSU	.0000	.0000	.0000
4	2	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSD	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	3	215 RE	.2599	1.1262	1.0784	105 RW	.0000	.0000	.0000
		FSD	1.0426	1.3144	1.3568	FSU	.4327	.5391	.4098
2	3	15 RE	.0000	.0000	.0000	67 RW	.0000	.0000	.0000
		FSD	.2843	.4133	.2428	FSU	.2573	.3695	.2069
3	3	198 RE	.1329	.5803	.4917	54 RW	.0000	.0000	.0000
		FSD	1.4643	.9487	.9552	FSU	.3844	.4236	.3254
4	3	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSD	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	4	121 RE	.2868	1.1647	1.5084	143 RW	.0000	.0000	.0000
		FSD	1.3492	1.6393	1.7020	FSU	.4292	.5463	.63767
2	4	44 RE	.5299	2.1608	1.7181	31 RW	.0000	.0000	.0000
		FSD	.6246	.4686	.4660	FSU	.6206	.41131	.4974
3	4	121 RE	.1805	.6285	.5175	0 RW	.0000	.0000	.0000
		FSD	1.1286	.8724	.8648	FSU	.0000	.0000	.0000
4	4	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSD	.0000	.0700	.0600	FSU	.0000	.0000	.0000
1	5	63 RE	.5777	2.8634	5.2767	28 RW	.0000	.0000	.0000
		FSD	2.2388	1.9149	1.9194	FSU	.3851	.4845	.3588

 REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

2	5	81	RE	.3764	1.3393	1.0323	0	RW	.0000	.0000	.0000	
			FSU	.7779	.7130	.7004		FSU	.0000	.0000	.0000	
3	5	74	RE	.2718	.9259	.7228	0	RW	.0000	.0000	.0000	
			FSU	.7301	.4532	.4601		FSU	.0000	.0000	.0000	
4	5	0	RE	.0000	.0000	.0000	0	RW	.0000	.0000	.0000	
			FSU	.0000	.0000	.0000		FSU	.0000	.0000	.0000	
1	6	56	RE	1.5247	4.0845	12.7170	29	RW	.0000	.0000	.0000	
			FSU	2.2494	2.0317	2.0640		FSU	.1490	.5407	.1495	
2	6	63	RE	.4039	1.4154	1.0051	0	RW	.0000	.0000	.0000	
			FSU	.5467	.4466	.4278		FSU	.0000	.0000	.0000	
3	6	89	RE	.9286	.7993	.5789	0	RW	.0000	.0000	.0000	
			FSU	.5857	.3280	.2994		FSU	.0000	.0000	.0000	
4	6	0	RE	.0000	.0000	.0000	0	RW	.0000	.0000	.0000	
			FSU	.0000	.0000	.0000		FSU	.0000	.0000	.0000	
1	7	57	RE	3.2979	9.9621	26.8070	4	RW	.0000	.0000	.0000	
			FSU	1.8939	1.6967	1.7140		FSU	.2135	.5121	.1856	
2	7	43	RE	.7882	2.4010	1.5867	0	RW	.0000	.0000	.0000	
			FSU	.7231	.6494	.6652		FSU	.0000	.0000	.0000	
A3	3	7	110	RE	.2553	.9670	.6218	0	RW	.0000	.0000	
-E			FSU	.6715	.4559	.4218		FSU	.0000	.0000	.0000	
4	7	2	RE	.0000	.6419	.3568	0	RW	.0000	.0000	.0000	
			FSU	.0009	.0048	.0030		FSU	.0000	.0000	.0000	
1	8	272	RE	.9191	2.0498	1.3442	0	RW	.0000	.0000	.0000	
			FSU	1.0983	1.2598	1.1281		FSU	.0000	.0000	.0000	
2	8	153	RE	.4312	1.2123	.7509	0	RW	.0000	.0000	.0000	
			FSU	.6922	.8718	.7020		FSU	.0000	.0000	.0000	
3	8	126	RE	.3230	1.2769	.7449	0	RW	.0000	.0000	.0000	
			FSU	.7987	.6288	.5978		FSU	.0000	.0000	.0000	
4	8	0	RE	.0000	.0000	.0000	0	RW	.0000	.0000	.0000	
			FSU	.0000	.0000	.0000		FSU	.0000	.0000	.0000	

N = 2 E+B:L RATIOS OF OBSERVED TO VETTE

I	J	No	18-27	27-400	18-400	No	18-27	27-400	18-400
1	1	331 RE	.4668	1.8260	1.6170	0 RW	.0000	.0000	.0000
		FSO	1.3868	1.6461	1.5514	FSO	.0000	.0000	.0000
2	1	111 RE	.5417	1.6951	1.3908	0 RW	.0000	.0000	.0000
		FSO	1.5357	1.11932	1.0660	FSO	.0000	.0000	.0000
3	1	32 RE	.5778	2.5545	3.0259	0 RW	.0000	.0000	.0000
		FSO	2.1478	.8603	.8400	FSO	.0000	.0000	.0000
4	1	0 RE	.0000	.0000	.0000	0 RW	.0000	.0100	.0000
		FSO	.0000	.0000	.0000	FSO	.0000	.0000	.0000
1	2	270 RE	.2592	1.1197	1.0045	0 RW	.0000	.0000	.0000
		FSO	1.0550	1.3063	1.3385	FSO	.0000	.0000	.0000
2	2	7 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSO	.2215	.5444	.1491	FSO	.0000	.0500	.0000
3	2	165 RE	.1149	.8016	.6781	0 RW	.0000	.0100	.0000
		FSO	1.9975	.9482	.9381	FSO	.0000	.0000	.0000
AB-6	4	2 0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSO	.0000	.0000	.0000	FSO	.0000	.0100	.0000
1	3	215 RE	.2825	1.2182	1.1644	105 RW	.0000	.0100	.0000
		FSO	1.0333	1.3016	1.3411	FSO	.4127	.5391	.4098
2	3	15 RE	.0000	.0000	.0000	67 RW	.0000	.0000	.0000
		FSO	.2843	.4133	.2428	FSO	.2573	.3695	.2069
3	3	198 RE	.1321	.5780	.4895	54 RW	.0000	.0000	.0000
		FSO	1.3474	.7846	.7908	FSO	.3844	.4236	.3254
4	3	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSO	.0000	.0000	.0000	FSO	.0000	.0000	.0000
1	4	121 RE	.3138	1.2378	1.5752	143 RW	.0000	.0000	.0000
		FSO	1.1365	1.6566	1.7396	FSO	.4292	.5463	.3767
2	4	44 RE	.4654	1.9018	1.5113	31 RW	.0000	.0000	.0000
		FSO	.5443	.3578	.3535	FSO	.6206	.4031	.4974
3	4	121 RE	.1769	.6140	.5060	0 RW	.0000	.0000	.0000
		FSO	.9974	.6898	.6869	FSO	.0000	.0000	.0000
4	4	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSO	.0000	.0000	.0000	FSO	.0000	.0360	.0000
1	5	63 RE	.5923	2.8025	4.7084	28 RW	.0000	.0000	.0000
		FSO	2.1804	1.7433	1.4624	FSO	.3851	.4845	.3588

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

2	5	81	RE	.3644	1.3087	1.0074	0	Rw	.0000	.0000	.0000	
			FSU	.6739	.5905	.5783		FSU	.0000	.0000	.0000	
3	5	74	RE	.2611	.8842	.6915	0	Rw	.0000	.0000	.0000	
			FSU	.6634	.3478	.3529		FSU	.0000	.0000	.0000	
4	5	0	RE	.0000	.0000	.0000	0	Rw	.0000	.0000	.0000	
			FSU	.0000	.0000	.0000		FSU	.0000	.0000	.0000	
1	6	56	RE	1.2126	4.1549	6.0608	29	Rw	.0000	.0000	.0000	
			FSU	2.0091	1.4512	1.0065		FSU	.1490	.5407	.1495	
2	6	63	RE	.3977	1.3817	.9895	0	Rw	.0000	.0000	.0000	
			FSU	.4941	.3745	.3560		FSU	.0000	.0000	.0000	
3	6	89	RE	.2462	.8575	.6217	0	Rw	.0000	.0000	.0000	
			FSU	.5604	.3206	.2907		FSU	.0000	.0000	.0000	
4	6	0	RE	.0000	.0000	.0000	0	Rw	.0000	.0000	.0000	
			FSU	.0000	.0000	.0000		FSU	.0000	.0000	.0000	
1	7	57	RE	1.8953	4.6865	5.9158	4	Rw	.0000	.0000	.0000	
			FSU	1.4637	.8751	.3106		FSU	.2135	.5121	.1856	
A3-7	2	7	43	RE	.7596	2.3047	1.5261	0	Rw	.0000	.0000	.0000
			FSU	.5734	.5255	.4961		FSU	.0000	.0000	.0000	
3	7	110	RE	.2809	1.0619	.6842	0	Rw	.0000	.0000	.0000	
			FSU	.2683	.4521	.4122		FSU	.0000	.0000	.0000	
4	7	2	RE	.0000	.6879	.3821	0	Rw	.0000	.0000	.0000	
			FSU	.0006	.0046	.0028		FSU	.0000	.0000	.0000	
1	8	272	RE	.9174	2.0312	1.3526	0	Rw	.0000	.0000	.0000	
			FSU	.9381	1.0950	.9657		FSU	.0000	.0000	.0000	
2	8	153	RE	.4653	1.3080	.8103	0	Rw	.0000	.0000	.0000	
			FSU	.4751	.8171	.6850		FSU	.0000	.0000	.0000	
3	8	126	RE	.3441	1.3457	.7941	0	Rw	.0000	.0000	.0000	
			FSU	.7625	.5826	.5487		FSU	.0000	.0000	.0000	
4	8	0	RE	.0000	.0000	.0000	0	Rw	.0000	.0000	.0000	
			FSU	.0000	.0000	.0000		FSU	.0000	.0000	.0000	

M# 4 E.H.L RATIOS OF OBSERVED TU VETTE

I	J	NO	18-27	27-400	18-400	NO	18-27	27-400	18-400
1	1	331 RE	.4041	1.6312	1.4500	0 RW	.0000	.0000	.0000
		FSU	1.1803	1.3002	1.2957	FSU	.0000	.0000	.0000
2	1	111 RE	.5074	1.5084	1.3157	0 RW	.0000	.0000	.0000
		FSU	1.5057	1.4596	1.0331	FSU	.0000	.0000	.0000
3	1	32 RE	.4490	2.7182	2.3613	0 RW	.0000	.0000	.0000
		FSU	2.1019	.7335	.7104	FSU	.0000	.0000	.0000
4	1	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	2	270 RE	.2715	1.1674	1.0506	0 RW	.0000	.0000	.0000
		FSU	.9916	1.2171	1.2406	FSU	.0000	.0000	.0000
2	2	7 RE	.6000	.6000	.6000	0 RW	.0000	.0000	.0000
		FSU	.2215	.5444	.1491	FSU	.0000	.0000	.0000
3	2	165 RE	.1077	.7519	.4359	0 RW	.0000	.0000	.0000
		FSU	1.9137	.7445	.7459	FSU	.0000	.0000	.0000
4	2	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	3	215 RE	.3014	1.2602	1.1953	105 RW	.0000	.0000	.0000
		FSU	.9932	1.2630	1.2921	FSU	.4127	.5391	.4098
2	3	15 RE	.0000	.0000	.0000	67 RW	.0000	.0000	.0000
		FSU	.2843	.4133	.2428	FSU	.2573	.3695	.2069
3	3	198 RE	.1341	.5874	.4974	54 RW	.0000	.0000	.0000
		FSU	1.2745	.6595	.6654	FSU	.3844	.4236	.3254
4	3	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	4	121 RE	.3251	1.1916	1.4470	143 RW	.69.8980	10.0779	25.8303
		FSU	1.2758	1.5766	1.6012	FSU	1.6181	1.4508	1.6033
2	4	44 RE	.4335	1.7732	1.4087	38 RW	161.6726	11.1916	50.9516
		FSU	.5172	.3154	.3106	FSU	2.2439	2.1936	2.2129
3	4	121 RE	.1786	.6194	.5106	0 RW	.0000	.0000	.0000
		FSU	.9189	.5670	.5644	FSU	.0000	.0000	.0000
4	4	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	5	63 RE	.4874	1.6925	1.9796	28 RW	.0000	.0100	.11000
		FSU	1.8126	.8459	.4139	FSU	.3841	.4845	.63588

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

2	5	81	RE	.3604	1.2913	.4924	0	RW	.0000	.0000	.0000
			FSU	.6266	.5304	.5187	-	FSU	.0000	.0000	.0000
3	5	74	RE	.2597	8739	.6844	0	RW	.0000	.0000	.0000
			FSU	.6746	.2790	.2811	-	FSU	.0000	.0000	.0000
4	5	0	RE	.0000	.0000	.0000	0	RW	.0000	.0000	.0000
			FSU	.0000	.0000	.0000	-	FSU	.0000	.0000	.0000
1	6	56	RE	.8123	2.1182	2.0902	29	RW	.0000	.0000	.0000
			FSU	1.5103	.6188	.3233	-	FSU	.1490	.5407	.1495
2	6	63	RE	.3695	1.3498	.9677	0	RW	.0000	.0000	.0000
			FSU	.4715	.3463	.3241	-	FSU	.0000	.0000	.0000
3	6	89	RE	.2617	.9143	.6626	0	RW	.0000	.0000	.0000
			FSU	.5713	.3157	.2734	-	FSU	.0000	.0000	.0000
4	6	0	RE	.0000	.0000	.0000	0	RW	.0000	.0000	.0000
			FSU	.0000	.0000	.0000	-	FSU	.0000	.0000	.0000
1	7	57	RE	1.2508	2.6690	2.5889	4	RW	.0000	.0000	.0000
			FSU	1.1773	.4531	.3867	-	FSU	.2135	.5121	.1856
2	7	43	RE	.7391	2.2362	1.4828	0	RW	.0000	.0000	.0000
			FSU	.4956	.4397	.4143	-	FSU	.0000	.0000	.0000
3	7	130	RE	.31159	1.1584	.7450	0	RW	.0000	.0000	.0000
A3-9			FSU	.6630	.4447	.4090	-	FSU	.0000	.0000	.0000
4	7	2	RE	.0000	.7220	.4013	0	RW	.0000	.0000	.0000
			FSU	.0002	.0742	.0825	-	FSU	.0000	.0000	.0000
1	8	272	RE	.9060	1.9904	1.3362	0	RW	.0000	.0000	.0000
			FSU	.8161	.9718	.8380	-	FSU	.0000	.0000	.0000
2	8	153	RE	.50129	1.4127	.8756	0	RW	.0000	.0000	.0000
			FSU	.6627	.7985	.6734	-	FSU	.0000	.0000	.0000
3	8	126	RE	.3651	1.4401	.8430	0	RW	.0000	.0000	.0000
			FSU	.7357	.5470	.5109	-	FSU	.0000	.0000	.0000
4	8	0	RL	.0000	.0000	.0000	0	RW	.0000	.0000	.0000
			FSU	.0000	.0000	.0000	-	FSU	.0000	.0000	.0000

H E E,B,L RATIOS OF OBSERVED TO VETTE

I	J	NO	18-27	27-400	18-400	HO	18-27	27-400	18-400
1	1	331 RE	.3679	1.5147	1.3496	0 KW	.0000	.0000	.0000
		FSO	1.0727	1.1641	1.1534		.0000	.0000	.0000
2	1	111 RE	.4848	1.4666	1.2811	0 RW	.0000	.0000	.0000
		FSO	1.4702	1.0390	1.0145		.0000	.0000	.0000
3	1	32 RE	.3885	2.4143	2.0511	0 KW	.0000	.0000	.0000
		FSO	2.0823	.6756	.6514		.0000	.0000	.0000
4	1	0 RE	.0000	.0000	.0000	0 KW	.0000	.0000	.0000
		FSO	.0000	.0000	.0000		.0000	.0000	.0000
1	2	270 RE	.2800	1.1923	1.1699	0 RW	.0000	.0000	.0000
		FSO	.9174	1.1143	1.1273		.0000	.0000	.0000
2	2	7 RE	.0000	.0000	.0000	0 KW	.0000	.0000	.0000
		FSO	.2215	.5444	.1491		.0000	.0000	.0000
3	2	165 RE	.1036	.7241	.6123	0 RW	.0000	.0000	.0000
		FSO	1.8690	.6246	.6234		.0000	.0000	.0000
A3	4	2 0 RE	.0100	.0000	.0000	0 KW	.0000	.0000	.0000
		FSO	.0100	.0000	.0000		.0000	.0000	.0000
O	1	3 215 RE	.3156	1.2661	1.1887	105 KW	47.2451	5.0345	15.1527
		FSO	.9311	1.1990	1.2126		.9697	1.0156	.9568
2	3	15 RE	.0000	.0000	.0000	67 RW	15n.36n6	15.7879	45.5786
		FSO	.2841	.4133	.2428		1.2412	1.2644	1.2278
3	3	19H RE	.1380	.6143	.5118	54 RW	.0000	.0100	.0000
		FSO	1.2266	.5673	.5731		.3864	.4236	.3254
4	3	0 RE	.0000	.0000	.0000	0 KW	.0000	.0000	.0000
		FSO	.0000	.0000	.0000		.0000	.0000	.0000
1	4	121 RE	.3230	1.0636	1.2147	143 KW	11.4122	1.4081	4.1464
		FSO	1.1717	1.4419	1.3647		.7422	.8457	.7047
2	4	44 RE	.4197	1.7181	1.3647	31 KW	23.30n5	1.6173	7.3573
		FSO	.50n3	.2945	.2934		1.3414	1.2460	1.2893
3	4	121 RE	.1834	.6354	.5239	0 KW	.0000	.0000	.0000
		FSO	.8685	.4789	.4764		.0000	.0000	.0000
4	4	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSO	.0000	.0000	.0000		.0000	.0000	.0000
1	5	63 RE	.4024	1.1470	1.1684	28 KW	.0000	.0000	.0000
		FSO	1.5537	.4453	.2703		.3851	.4845	.3588

2	5	81	RE	+3611	1.2952	+9958	0	RW	+0000	+0000	+0000
			FSU	+6033	+4987	+4877		FSU	+0000	+0000	+0000
3	5	74	RE	+2624	+8827	+6919	0	RW	+0000	+0000	+0000
			FSU	+4036	+2416	+2391		FSU	+0000	+0000	+0000
4	5	0	RE	+0000	+0000	+0000	0	RW	+0000	+0000	+0000
			FSU	+0000	+0000	+0000		FSU	+0000	+0000	+0000
1	6	56	RE	+4177	1.4208	1.2534	29	RW	+0000	+0000	+0000
			FSU	+2915	+3850	+3702		FSU	+1490	+4407	+1495
2	6	63	RE	+3844	1.3435	+9634	0	RW	+0000	+0000	+0000
			FSU	+4601	+3319	+3142		FSU	+0000	+0000	+0000
3	6	89	RE	+2798	+9767	+7080	0	RW	+0000	+0000	+0000
			FSU	+5654	+2966	+2622		FSU	+0000	+0000	+0000
4	6	0	RE	+0000	+0000	+0000	0	RW	+0000	+0000	+0000
			FSU	+0000	+0100	+0000		FSU	+0000	+0000	+0000
1	7	57	RE	+9728	1.9369	1.7124	4	RW	+0000	+0000	+0000
			FSU	+0612	+3436	+4657		FSU	+2135	+5121	+1856
2	7	43	RE	+7345	2.2181	1.4722	0	RW	+0000	+0000	+0000
			FSU	+4506	+3900	+3489		FSU	+0000	+0000	+0000
3	7	110	RE	+3325	1.2589	+8097	0	RW	+0000	+0000	+0000
			FSU	+6586	+4385	+4020		FSU	+0000	+0000	+0000
4	7	2	RE	+0000	+7590	+4219	0	RW	+0000	+0000	+0000
			FSU	+0000	+0039	+0021		FSU	+0000	+0000	+0000
1	R	272	RE	+9065	1.9776	1.3363	0	RW	+0000	+0000	+0000
			FSU	+7413	+9000	+7594		FSU	+0000	+0000	+0000
2	8	153	RE	+5447	1.5277	+9471	0	RW	+0000	+0000	+0000
			FSU	+6546	+7939	+6667		FSU	+0000	+0000	+0000
3	8	126	RE	+3885	1.5334	+8972	0	RW	+0000	+0000	+0000
			FSU	+7166	+5204	+4827		FSU	+0000	+0000	+0000
4	B	0	RE	+0000	+0000	+0000	0	RW	+0000	+0000	+0000
			FSU	+0000	+0000	+0000		FSU	+0000	+0000	+0000

M= 4 E,H,L RATIOS OF OBSERVED TU VETTE

I	J	NO	18-27	27-400	18-400	NU	18-27	27-400	18-400
1	1	331 RE	.3481 FSU	1.4618 1.0159	1.2954 1.0780	0 R _u FSU	.00000 .00000	.00000 .00000	.00000 .00000
2	1	111 RE	.4728 FSU	1.4998 1.451n	1.2773 1.0237	0 R _u FSU	.00000 .00700	.00000 .00000	.00000 .00000
3	1	32 RE	.3575 FSU	2.2306 2.071?	1.8948 .6432	0 R _u FSU	.00000 .00000	.00000 .00000	.00000 .00010
4	1	n RE	.0100 FSU	.0000 .0000	.0000 .0100	0 R _u FSU	.00000 .00000	.00000 .00000	.00000 .00000
1	2	270 RE	.2873 FSU	1.2n84 .8536	1.0809 1.0702	0 R _u FSU	.00000 .00000	.00000 .00000	.00000 .00000
2	2	7 RE	.00000 FSU	.00000 .2215	.00000 .5444	0 R _u FSU	.00000 .00000	.00000 .00000	.00000 .00000
3	2	165 RE	.1020 FSU	.7137 1.8445	.6034 .5476	0 R _u FSU	.00000 .00000	.00000 .00000	.00000 .00000
A312	4	2 n RE	.00000 FSU	.00000 .00000	.00000 .00000	0 R _u FSU	.00000 .00000	.00000 .00000	.00000 .00000
	1	3 215 RE	.1277 FSU	1.2657 1.0713	1.1777 1.0421	105 R _u FSU	16.6423 .7924	1.7499 1.8523	E 3065 1.7800
	2	3 15 RE	.00000 FSU	.00000 .2843	.00000 .4133	67 R _u FSU	32.4659 .50119	3.2956 .5376	9 5943 .4495
	3	3 198 RE	.1429 FSU	.6757 1.1963	.5299 .5030	54 R _u FSU	66.5025 .5926	7.9345 .5925	19' 1823 .5321
	4	3 n RE	.00000 FSU	.00000 .00000	.00000 .00000	0 R _u FSU	.00000 .00000	.00000 .0350	.00000 .00000
	1	4 121 RE	.3198 FSU	.9618 1.0812	1.0514 1.0595	143 R _u FSU	5.4523 .6947	.7663 .7664	1.9771 .6581
	2	4 44 RE	.418n FSU	1.7117 .5754	1.1594 .2925	31 R _u FSU	11.4550 1.3318	.8087 1.2453	1.6794 1.2790
	3	4 121 RE	.1900 FSU	.6579 .8364	.5425 .4167	0 R _u FSU	.00000 .00000	.00000 .00000	.00000 .00000
	4	4 n RE	.00000 FSU	.00000 .00000	.00000 .00000	0 R _u FSU	.00000 .00000	.00000 .00000	.00000 .00000
	1	5 63 RE	.3474 FSU	.8810 1.4077	.843n 3.304	28 R _u FSU	298.7222 1.9642	17.1516 1.9818	105.64590 1.9561

 REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

2	5	81	RE	.3677	1.3716	1.0144	0	Rw	.0000	.0000	.0000	
			FSU	.5918	.4819	.4715		FSU	.0000	.0000	.0000	
3	5	74	RE	.2648	.9750	.7094	0	Rw	.0000	.0000	.0000	
			FSU	.5936	.2240	.2141		FSU	.0000	.0000	.0000	
4	5	0	RE	.0100	.0000	.0000	0	Rw	.0000	.0000	.0000	
			FSU	.0000	.0100	.0000		FSU	.0000	.0000	.0000	
1	6	56	RE	.5173	1.1125	.9345	29	Rw	117.1446	10.3573	5A.5195	
			FSU	1.1926	.3357	.4182		FSU	.7139	.8794	.7104	
2	6	63	RE	.3944	1.3629	.9782	0	Rw	.0000	.0000	.0000	
			FSU	.4534	.3248	.2999		FSU	.0000	.0000	.0000	
3	6	89	RE	.2994	1.0443	.7572	0	Rw	.0000	.0000	.0000	
			FSU	.5628	.2934	.2577		FSU	.0000	.0000	.0000	
4	6	0	RE	.0000	.0000	.0000	0	Rw	.0000	.0000	.0000	
			FSU	.0000	.0000	.0000		FSU	.0000	.0000	.0000	
1	7	57	RE	.8344	1.5973	1.3483	4	Rw	92.6496	10.1541	4A.6903	
			FSU	1.01172	.3277	.5165		FSU	.2154	.5124	.1876	
2	7	43	RE	.7437	2.2429	1.4897	0	Rw	.0000	.0000	.0000	
			FSU	.4232	.3595	.3134		FSU	.0000	.0000	.0000	
A3-13	3	7	110	RE	.3603	1.3643	.8774	0	Rw	.0000	.0000	.0000
			FSU	.6556	.4343	.3973		FSU	.0000	.0000	.0000	
4	7	2	RE	.0000	.8015	.4456	0	Rw	.0000	.0000	.0000	
			FSU	.0003	.0137	.0019		FSU	.0000	.0000	.0000	
1	8	272	RE	.9175	1.9904	1.3515	0	Rw	.0000	.0000	.0000	
			FSU	.6988	.8615	.7152		FSU	.0000	.0000	.0000	
2	8	153	RE	.5876	1.6486	1.0225	0	Rw	.0000	.0000	.0000	
			FSU	.4499	.7917	.6628		FSU	.0000	.0000	.0000	
3	8	126	RE	.4139	1.6349	.9562	0	Rw	.0000	.0000	.0000	
			FSU	.7037	.5018	.4629		FSU	.0000	.0000	.0000	
4	8	0	RE	.0000	.0000	.0000	0	Rw	.0000	.0000	.0000	
			FSU	.0000	.0000	.0000		FSU	.0000	.0000	.0000	

MW 7 E.O.L RATIOS OF OBSERVED TO VETIE

1	J	NO	18-27	27-400	18-400	NO	18-27	27-400	18-400
1	1	331 RE FSU	.3342 9683	1.4146 1.0772	1.2641 1.0197	0 R ₁ FSU	.0000 .0000	.0000 .0000	.0000 .0000
2	1	111 RE FSU	.4673 1.4127	1.5616 1.5012	1.3184 1.9837	0 RW FSU	.0000 .0000	.0000 .0000	.0000 .0000
3	1	32 RE FSU	.3341 2.0583	2.0944 1.6180	1.7834 1.5837	0 RW FSU	.0000 .0000	.0000 .0000	.0000 .0000
4	1	0 RE FSU	.0000 .0000	.0000 .0000	.0000 .0000	0 RW FSU	.0000 .0000	.0000 .0000	.0000 .0000
1	2	270 RE FSU	.3005 1.7721	1.2349 1.9339	1.00984 1.9274	0 RW FSU	.0000 .0000	.0000 .0000	.0000 .0000
2	2	7 RE FSU	15.9072 1.2248	1.6532 1.5459	3.7574 1.541	0 R ₇ FSU	.0000 .0000	.0000 .0000	.0000 .0000
3	2	165 RE FSU	.1032 1.8231	.7224 1.4107	.6107 1.4693	0 RW FSU	.0000 .0000	.0000 .0000	.0000 .0000
A3	4	2 0 RE FSU	.0000 .0000	.0000 .0001	.0000 .0000	0 RW FSU	.0000 .0000	.0000 .0000	.0000 .0000
14	1	3 215 RE FSU	.3476 1.7834	1.2477 1.0716	1.1644 1.0568	105 RW FSU	5.7949 1.6069	.6098 1.6879	1.8410 1.5949
2	3	15 RE FSU	22.2330 1.3077	1.1764 1.4216	5.7071 1.2591	67 RW FSU	10.1377 1.3957	1.0247 1.4521	2.9858 1.3393
3	3	198 RE FSU	.1539 1.1664	.6738 1.4129	.5716 1.4384	54 RW FSU	1.67064 1.5045	1.9836 1.5118	4.8660 4.388
4	3	0 RE FSU	.0000 .0000	.0000 .0020	.0000 .0000	0 RW FSU	.0000 .0000	.0000 .0000	.0000 .0000
1	4	121 RE FSU	.3165 1.9662	.8433 1.3004	.8744 1.1828	143 RW FSU	2.4119 1.5714	.3433 1.6683	6.8849 5.369
2	4	44 RE FSU	.4327 1.5055	1.7731 1.2907	1.40186 1.2867	31 RW FSU	5.0572 1.0446	.3524 1.9422	1.6016 1.9848
3	4	121 RE FSU	.2056 1.8028	.7113 1.3449	.6866 1.3415	0 RW FSU	.0000 .0000	.0000 .0000	.0000 .0000
4	4	0 RE FSU	.0000 .0000	.0000 .0000	.0000 .0000	0 RW FSU	.0000 .0000	.0000 .0000	.0000 .0000
5	5	63 RE FSU	.2914 1.2819	.6668 1.3336	.5961 1.4161	28 RW FSU	16.1669 1.4300	.9475 1.5432	5.9638 6.4237

2	5	81	RE FSU	.3402 5837	1.4633 4690	1.1774 4593	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
3	5	74	RE FSU	.2648 5674	.9648 2190	.7613 2113	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
4	5	0	RE FSU	.0000 .0000	.0000 .0000	.0000 .0000	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
1	6	56	RE FSU	.4290 1.1186	.8631 3537	.6948 4672	29 FSU	Rw FSU	17.8A99 .1677	1.4980 .5428	A.2894 .1544	
2	6	63	RE FSU	.4142 4482	1.4428 3201	1.0362 .2935	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
3	6	89	RE FSU	.3389 5620	1.1813 2948	.9568 .7579	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
4	6	0	RE FSU	.0000 .0000	.0000 .0000	.0000 .0000	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
1	7	57	RE FSU	.7180 9638	1.3185 3498	1.0640 .6461	4 FSU	Rw FSU	19.2866 .2136	2.1132 .5121	1n.1345 .1856	
2	7	43	RE FSU	.7842 3956	2.3610 3290	1.5695 .2771	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
A3-15	3	7	110	RE FSU	.4149 6524	1.5712 4299	1.0105 .3922	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000
4	7	2	RE FSU	.0000 .0000	.8928 8034	.4962 .0016	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
1	8	272	RE FSU	.9576 6670	2.0612 8357	1.4086 .6828	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
2	8	153	RE FSU	.6726 6457	1.8458 7903	1.1701 .6597	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
3	8	126	RE FSU	.4654 6894	1.8411 4803	1.1743 .4473	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
4	8	0	RE FSU	.0000 .0000	.0000 .0000	.0000 .0000	0 FSU	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	

7

V

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

H ₂ R E:O:L RATIOS OF OBSERVED TO VETTE									
I	J	NO	18-27	27-400	18-400	NO	18-27	27-400	18-400
1	1	331 RE	.3348	1.4276	1.2767	0 RW	.0000	.0000	.0000
		FSU	.9528	1.0230	1.0059	FSU	.0000	.0000	.0000
2	1	111 RE	.4724	1.5664	1.3797	0 RW	.0000	.0000	.0000
		FSU	1.3889	.9868	.9718	FSU	.0000	.0000	.0000
3	1	32 RE	.3306	2.0896	1.7754	0 RW	.0000	.0000	.0000
		FSU	2.0511	.5895	.5644	FSU	.0000	.0000	.0000
4	1	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	2	270 RE	.3122	1.2617	1.1183	0 RW	.0000	.0000	.0000
		FSU	.7357	.8984	.8875	FSU	.0000	.0000	.0000
2	2	7 RE	6.0157	.2471	1.4210	0 RW	.0000	.0000	.0000
		FSU	.2219	.5446	.1497	FSU	.0000	.0000	.0000
3	2	165 RE	.1065	.7459	.6304	0 RW	.0000	.0000	.0000
		FSU	1.8158	.4418	.4402	FSU	.0000	.0000	.0000
4	2	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
16	1	3 215 RE	.3632	1.2772	1.1641	105 RW	3.4898	.3664	1.1066
		FSU	.7355	1.0431	1.0214	FSU	.5221	.6171	.5104
2	3	15 RE	7.7813	.4114	1.9962	67 RW	5.8689	.5924	1.7267
		FSU	.2992	.4172	.2513	FSU	.3607	.4262	.3027
3	3	198 RE	.1644	.7198	.6095	54 RW	8.7685	1.0383	2.5133
		FSU	1.1549	.4038	.4092	FSU	.4800	.4905	.4131
4	3	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	4	121 RE	.3176	.7906	.7991	143 RW	1.6508	.2334	.6013
		FSU	.9129	1.2932	1.1722	FSU	.5122	.6215	.4764
2	4	44 RE	.4548	1.8643	1.4803	31 RW	3.2117	.2243	1.0187
		FSU	.5069	.2921	.2884	FSU	.8589	.7240	.7787
3	4	121 RE	.2207	.7633	.6296	0 RW	.0000	.0000	.0000
		FSU	.7882	.3096	.3061	FSU	.0000	.0000	.0000
4	4	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	5	63 RE	.2686	.5738	.5099	28 RW	6.9947	.4280	2.5831
		FSU	1.2442	.3707	.4533	FSU	.4054	.5190	.3944

2	5	81	RE	.4150	1.4975	1.1470	0	Rw	.0000	.0000	.0000
		FSU		.5826	.4662	.4569		FSU	.0000	.0000	.0000
3	5	74	RE	.3106	1.0379	.8150	0	Rw	.0000	.0000	.0000
		FSU		.5868	.2234	.2129		FSU	.0000	.0000	.0000
4	5	0	RE	.0000	.0000	.0000	0	Rw	.0000	.0000	.0000
		FSU		.0000	.0000	.0000		FSU	.0000	.0000	.0000
1	6	56	RE	.3972	.7747	.6124	29	Rw	8.4358	.7032	7.8988
		FSU		1.0957	.3803	.4895		FSU	.1519	.5462	.1544
2	6	63	RE	.4453	1.5346	1.1026	0	Rw	.0000	.0000	.0000
		FSU		.4464	.3199	.2923		FSU	.0000	.0000	.0000
3	6	89	RE	.3741	1.3034	.4456	0	Rw	.0000	.0000	.0000
		FSU		.5628	.2980	.2608		FSU	.0000	.0000	.0000
4	6	0	RE	.0000	.0000	.0000	0	Rw	.0000	.0000	.0000
		FSU		.0000	.0000	.0000		FSU	.0000	.0000	.0000
1	7	57	RE	.6805	1.2243	.9677	4	Rw	9.5909	1.0508	5.0395
		FSU		.9490	.3724	.5643		FSU	.2135	.5122	.1856
2	7	43	RE	.8316	2.5011	1.6633	0	Rw	.0000	.0000	.0000
		FSU		.3843	.3167	.2617		FSU	.0000	.0000	.0000
3	7	110	RE	.4625	1.7513	1.1263	0	Rw	.0000	.0000	.0000
		FSU		.6509	.4280	.3899		FSU	.0000	.0000	.0000
4	7	2	RE	.0000	.9769	.5430	0	Rw	.0000	.0000	.0000
		FSU		.0007	.0032	.0015		FSU	.0000	.0000	.0000
1	8	272	RE	1.00039	2.1508	1.4752	0	Rw	.0000	.0000	.0000
		FSU		.6630	.8349	.6797		FSU	.0000	.0000	.0000
2	8	153	RE	.7466	2.0924	1.2985	0	Rw	.0000	.0000	.0000
		FSU		.6446	.7905	.6591		FSU	.0000	.0000	.0000
3	8	126	RE	.5119	2.0250	1.1834	0	Rw	.0000	.0000	.0000
		FSU		.6828	.4698	.4294		FSU	.0000	.0000	.0000
4	8	0	RE	.0000	.0000	.0000	0	Rw	.0000	.0000	.0000
		FSU		.0000	.0000	.0000		FSU	.0000	.0000	.0000

ME 9 E,B,L RATIOS OF OBSERVED TO VETTE

I	J	NO	19-27	27-400	18-400	NO	18-27	27-400	18-400
1	1	331 RE	.3394	1.4415	1.7003	0 RW	.0000	.0000	.0000
		FSU	.9470	1.1201	1.0038	FSU	.0000	.0000	.0000
2	1	111 RE	.4797	1.6276	1.4369	0 RW	.0005	.0000	.0000
		FSU	1.3755	.9753	.9638	FSU	.0000	.0000	.0000
3	1	32 RE	.3329	2.1137	1.7967	0 RW	.0000	.0000	.0000
		FSU	2.0467	.5785	.5534	FSU	.0000	.0000	.0000
4	1	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	2	270 RE	.3220	1.2867	1.1377	0 RW	.0000	.0000	.0000
		FSU	.7206	.8873	.8748	FSU	.0000	.0000	.0000
2	2	7 RE	3.5658	.1464	.8423	0 RW	.0000	.0000	.0000
		FSU	.2215	.5444	.1491	FSU	.0000	.0000	.0000
3	2	165 RE	.1099	.7713	.6511	0 RW	.0000	.0000	.0000
		FSU	1.8130	.4304	.4288	FSU	.0000	.0000	.0000
A3-18	4	2 0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	3	215 RE	.3752	1.2891	1.1693	105 RW	2.6218	.2748	.8304
		FSU	.7109	1.0331	1.0082	FSU	.4748	.5796	.4641
2	3	15 RE	4.4615	.2358	1.1443	67 RW	4.3561	.4394	1.2810
		FSU	.2970	.4362	.2495	FSU	.3442	.4144	.2851
3	3	198 RE	.1732	.7583	.6421	54 RW	6.1581	.7295	1.7661
		FSU	1.1501	.3913	.3966	FSU	.4693	.4814	.4019
4	3	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	4	121 RE	.3205	.7667	.7643	143 RW	1.3285	.1882	.4846
		FSU	.8887	1.2969	1.1754	FSU	.4771	.5933	.4387
2	4	44 RE	.4756	1.9449	1.5481	31 RW	2.4263	.1696	.7700
		FSU	.5082	.2935	.2900	FSU	.7494	.5876	.6543
3	4	121 RE	.2335	.8071	.6658	0 RW	.0000	.0000	.0000
		FSU	.7809	.2916	.2877	FSU	.0000	.0000	.0000
4	4	0 RE	.0000	.0100	.0100	0 RW	.0000	.0000	.0000
		FSU	.0000	.0100	.0100	FSU	.0000	.0000	.0000
1	5	63 RE	.2585	.5168	.4720	28 RW	4.4381	.2718	1.6399
		FSU	1.2291	.3954	.4723	FSU	.3967	.5098	.3833

2	5	81	RE FSU	.4367 .5631	1.5724 .4661	1.2673 .4570	0	Rw FSU	.0000 .0001	.0000 .0000	.0060 .0000	
3	5	74	RE FSU	.3284 .5872	1.0945 .2240	.8613 .2165	0	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
4	5	0	RE FSU	.0700 .0000	.0000 .0000	.0000 .0000	0	Rw FSU	.0000 .0000	.0130 .0000	.0060 .0000	
1	6	56	RE FSU	.3845 1.0870	.7375 .3981	.5774 .5615	29	Rw FSU	5.0010 .1495	4659 .5495	2.5853 .1601	
2	6	63	RE FSU	.4692 .4458	1.6159 .3207	1.1613 .2924	0	Rw FSU	.0000 .0000	.0000 .0000	.0060 .0000	
3	6	89	RE FSU	.4027 .5637	1.4025 .3808	1.01175 .2634	0	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
4	6	0	RE FSU	.0000 .0000	.0000 .0000	.0000 .0000	0	Rw FSU	.0000 .0000	.0000 .0000	.0060 .0000	
1	7	57	RE FSU	.6684 .9429	1.1892 .3876	.9295 .5741	4	Rw FSU	6.5850 .2135	.7215 .5142	3.4610 .1857	
2	7	43	RE FSU	.8734 .3791	2.6242 .3113	1.2470 .2547	0	Rw FSU	.0000 .0000	.0000 .0000	.0060 .0000	
3	7	110	RE FSU	.5008 .4501	1.8941 .4771	1.2195 .3687	0	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
6	4	7	2	RE FSU	.0000 .0008	1.0461 .6031	.5814 .0014	0	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000
1	8	272	RE FSU	1.0454 .6659	2.2334 .8397	1.5352 .6838	0	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
2	8	153	RE FSU	.8060 .6445	2.2484 .7919	1.4017 .6592	0	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
3	8	126	RE FSU	.5495 .4794	2.1745 .4641	1.2706 .4236	0	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	
4	8	0	RE FSU	.0000 .0000	.0000 .0000	.0000 .0000	0	Rw FSU	.0000 .0000	.0000 .0000	.0000 .0000	

REPRODUCIBILITY OF THE
ORIGINAL PAGE IS POOR

MAIN E.H.L RATIOS OF OBSERVED TO VETTE

I	J	NU	18-27	27-400	18-400	NU	18-27	27-400	18-400
1	1	131 RE	.3446	1.4793	1.3238	0 RW	.0000	.0000	.0000
		FSU	.9447	1.704	1.0047	FSU	.0000	.0000	.0000
2	1	111 RE	.4866	1.6784	1.4842	0 RW	.0000	.0000	.0000
		FSU	1.3674	.9729	.9582	FSU	.0000	.0000	.0000
3	1	32 RE	.7366	2.1417	1.8220	0 RW	.0000	.0000	.0000
		FSU	2.0438	.5715	.5470	FSU	.0000	.0000	.0000
4	1	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	2	270 RE	.3298	1.3079	1.1546	0 RW	.0000	.0000	.0000
		FSU	.7145	.BH50	.6718	FSU	.0000	.0000	.0000
2	2	7 RE	2.6113	*1072	.6188	0 RW	.0000	.0000	.0000
		FSU	.2216	5444	.1491	FSU	.0000	.0000	.0000
3	2	165 RE	.1129	.7913	.6688	0 RW	.0000	.0000	.0000
		FSU	1.8119	.4256	.4240	FSU	.0000	.0000	.0000
A3-20	4	2 0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	3	215 RE	.3842	1.3002	1.1758	105 RW	2.2102	.2304	.6964
		FSU	.6981	1.0103	1.0038	FSU	.4497	.5608	.4398
2	3	15 RE	3.2112	*1647	.8236	67 RW	3.6426	.3673	1.0719
		FSU	.2982	.4154	.2488	FSU	.3354	.4080	.2755
3	3	198 RE	.1802	.7488	.6680	54 RW	4.9826	.5400	1.4286
		FSU	1.1477	.3456	.3908	FSU	.4636	.4765	.3961
4	3	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	4	121 RE	.3236	.7653	.7467	143 RW	1.1639	.1651	.4250
		FSU	.8770	1.3121	1.1804	FSU	.4573	.5769	.4164
2	4	44 RE	.4929	2.0208	1.6043	31 RW	2.0228	.1416	.6426
		FSU	.5091	.2946	.2913	FSU	.6926	.5111	.5869
3	4	121 RE	.2416	.8419	.6946	0 RW	.0000	.0000	.0000
		FSU	.7769	.2814	.2771	FSU	.0000	.0000	.0000
4	4	0 RE	.0000	.0000	.0000	0 RW	.0000	.0000	.0000
		FSU	.0000	.0000	.0000	FSU	.0000	.0000	.0000
1	5	63 RE	.2536	.5180	.4524	28 RW	3.3775	.2069	1.2484
		FSU	1.2224	.4110	.4832	FSU	.3428	.5054	.3781

2	5	81	RE	.4542	1.6359	1.2560	0	Rw	.0000	.0000	.0000	
			FSU	.5839	4.646	2.4577		FSU	.0000	.0000	.0000	
3	5	74	RE	.3422	1.1475	.8903	0	Rw	.0000	.0000	.0000	
			FSU	.5878	.2115	.2196		FSU	.0000	.0000	.0000	
4	5	7	RE	.0730	.0100	.0000	0	Rw	.0000	.0000	.0000	
			FSU	.0730	.0100	.0000		FSU	.0000	.0000	.0000	
1	6	56	RE	.3791	.7199	.5684	29	Rw	4.3778	.3637	2.0192	
			FSU	1.0831	.4797	.4687		FSU	.1497	.5519	.1650	
2	6	63	RE	.4845	1.6817	1.2084	0	Rw	.0000	.0000	.0000	
			FSU	.4456	.3215	.2929		FSU	.0000	.0000	.0000	
3	6	89	RE	.4250	1.4798	1.0737	0	Rw	.0000	.0000	.0000	
			FSU	.5644	.3728	.2654		FSU	.0000	.0000	.0000	
4	6	0	RE	.0000	.0000	.0000	0	Rw	.0000	.0000	.0000	
			FSU	.0101	.0001	.0000		FSU	.0000	.0000	.0000	
1	7	57	RE	.6658	1.1758	.9129	4	Rw	5.2589	.5762	2.7632	
			FSU	.9399	.3976	.5800		FSU	.2136	.5123	.1858	
2	7	43	RF	.9077	2.7279	1.8150	0	Rw	.0000	.0000	.0000	
			FSU	.3765	.3147	.2511		FSU	.0000	.0000	.0000	
A3-21	3	7	110	RE	.5304	2.0084	1.2914	0	Rw	.0000	.0000	.0000
			FSU	.4497	.4265	.3680		FSU	.0000	.0000	.0000	
	4	7	2	RE	.0000	1.1005	.6116	0	Rw	.0000	.0000	.0000
			FSU	.0009	.0131	.0013		FSU	.0000	.0000	.0000	
1	8	272	RE	1.0793	2.3015	1.6842	0	Rw	.0070	.0100	.0000	
			FSU	.6699	.8447	.6887		FSU	.0000	.0000	.0000	
2	8	153	RE	.8521	2.3472	1.4814	0	Rw	.0000	.0000	.0000	
			FSU	.4446	.7914	.4595		FSU	.0000	.0000	.0000	
3	8	126	RE	.5748	2.2912	1.3384	0	Rw	.0000	.0000	.0000	
			FSU	.6774	.4608	.4203		FSU	.0000	.0000	.0000	
4	8	0	RE	.0100	.0070	.0000	0	Rw	.0000	.0000	.0000	
			FSU	.0100	.0000	.0000		FSU	.0000	.0000	.0000	